

# Three Phase Theory



***POWERMETRIX***

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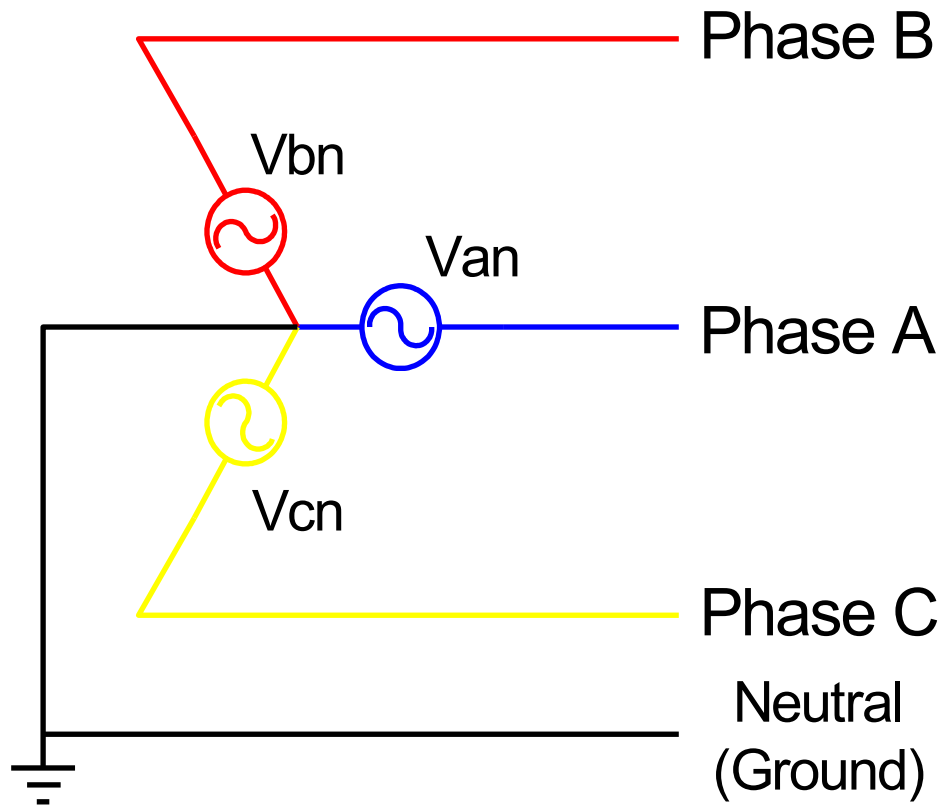
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***POWERMETRIX***

# Three Phase Power

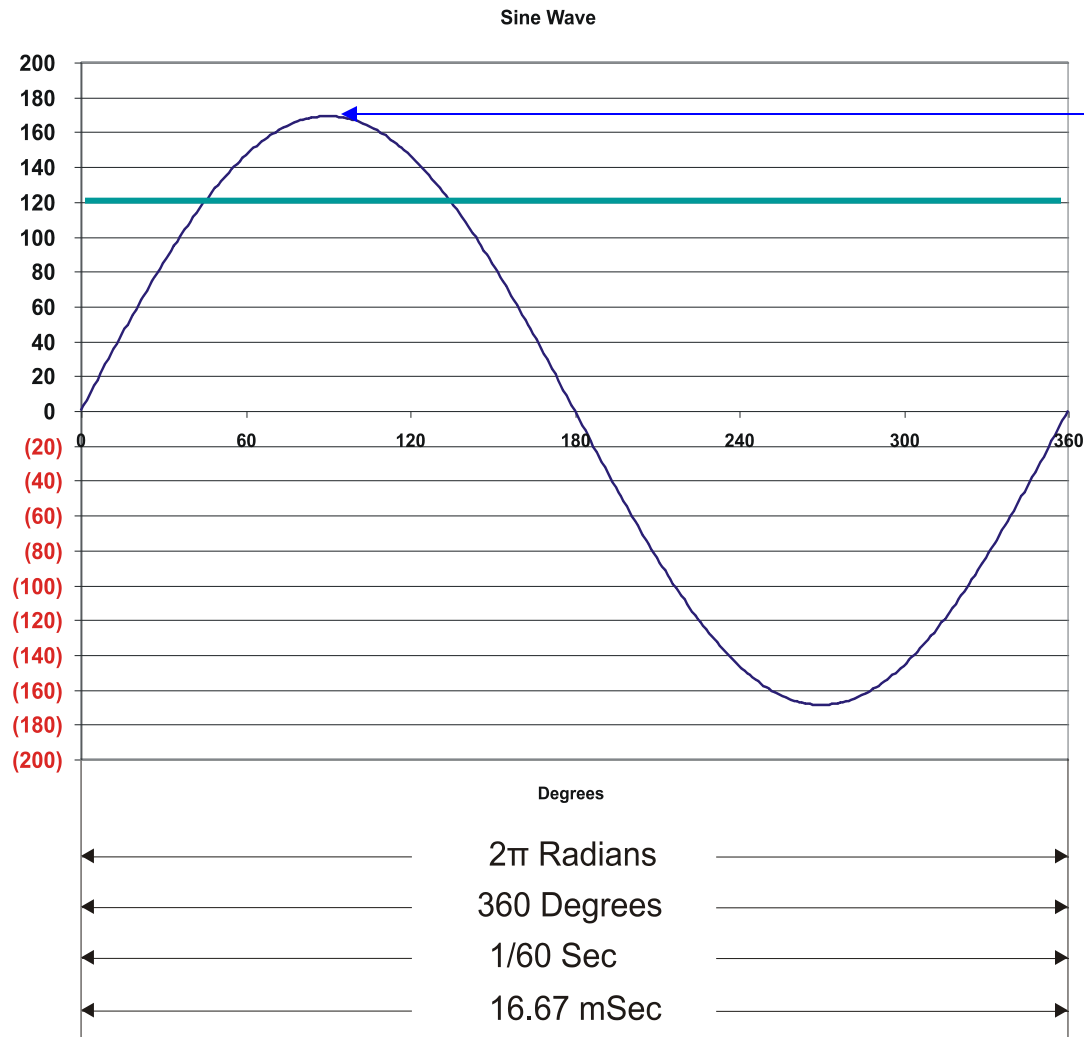
## Introduction



### Basic Assumptions

- Three AC voltage sources
- Voltages Displaced in time
- Each sinusoidal
- Identical in Amplitude

# AC Theory – Sine Wave



$$V = V_{pk} \sin(2\pi ft - \theta)$$

$$V_{pk} = \sqrt{2} V_{rms}$$

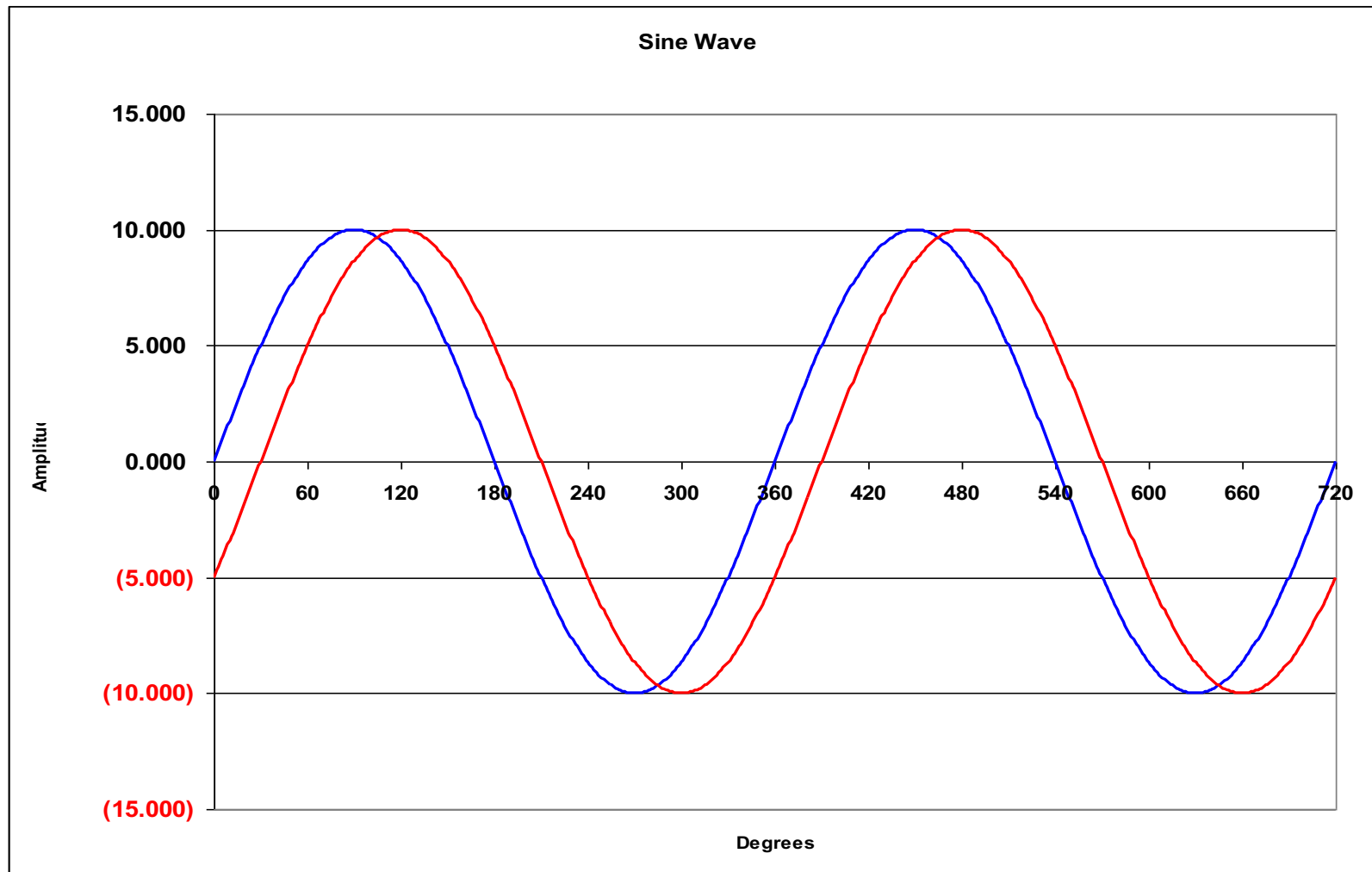
$$V_{rms} = 120$$

$$V_{pk} = 169$$

$$f = 1 / \text{time}$$

$$\theta = 0$$

# AC Theory - Phase

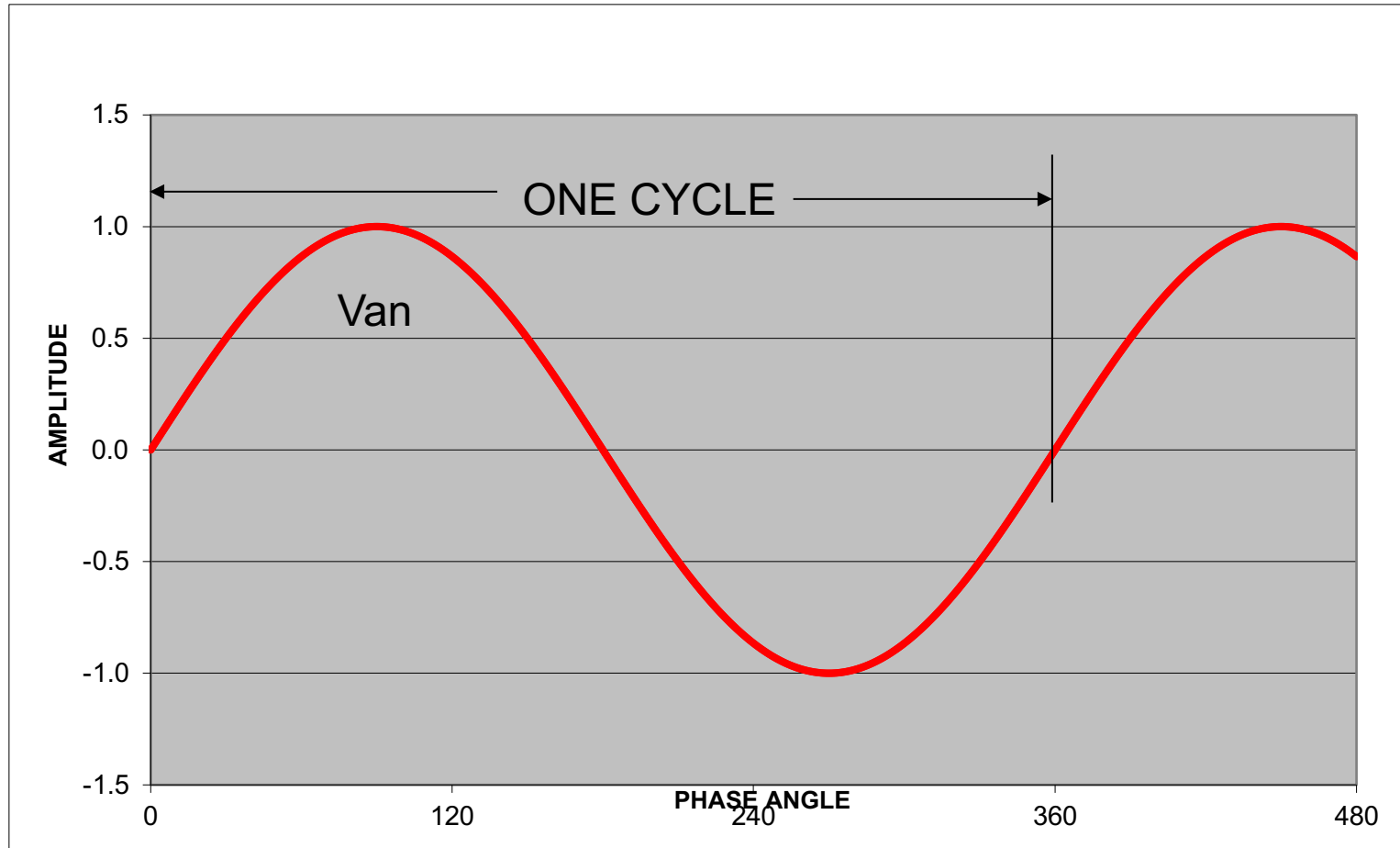


$$V = 10\text{Sin}(2\pi ft)$$

$$V = 10\text{Sin}(2\pi ft - 30)$$

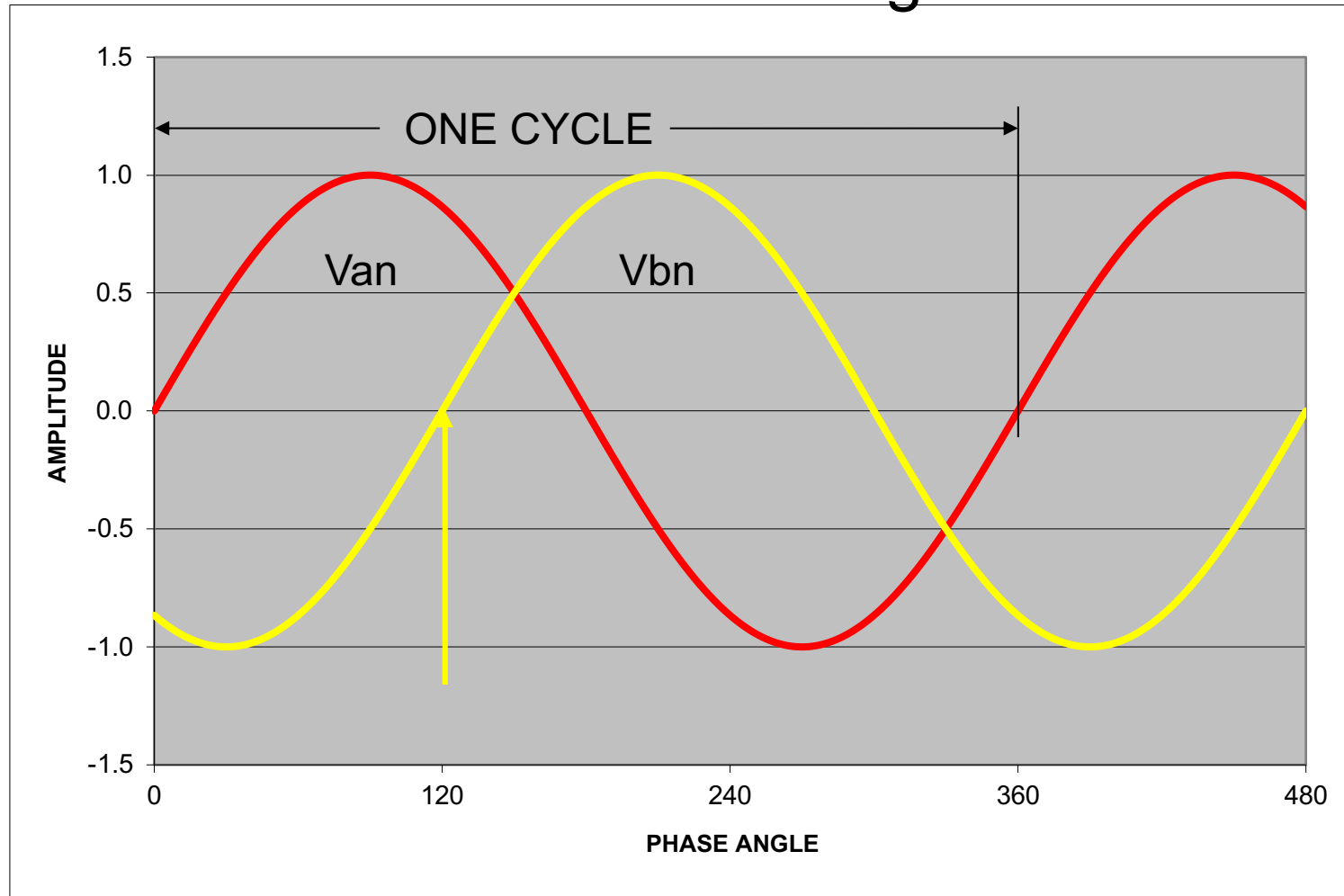
# Three Phase Theory

## Single Phase - Voltage Plot



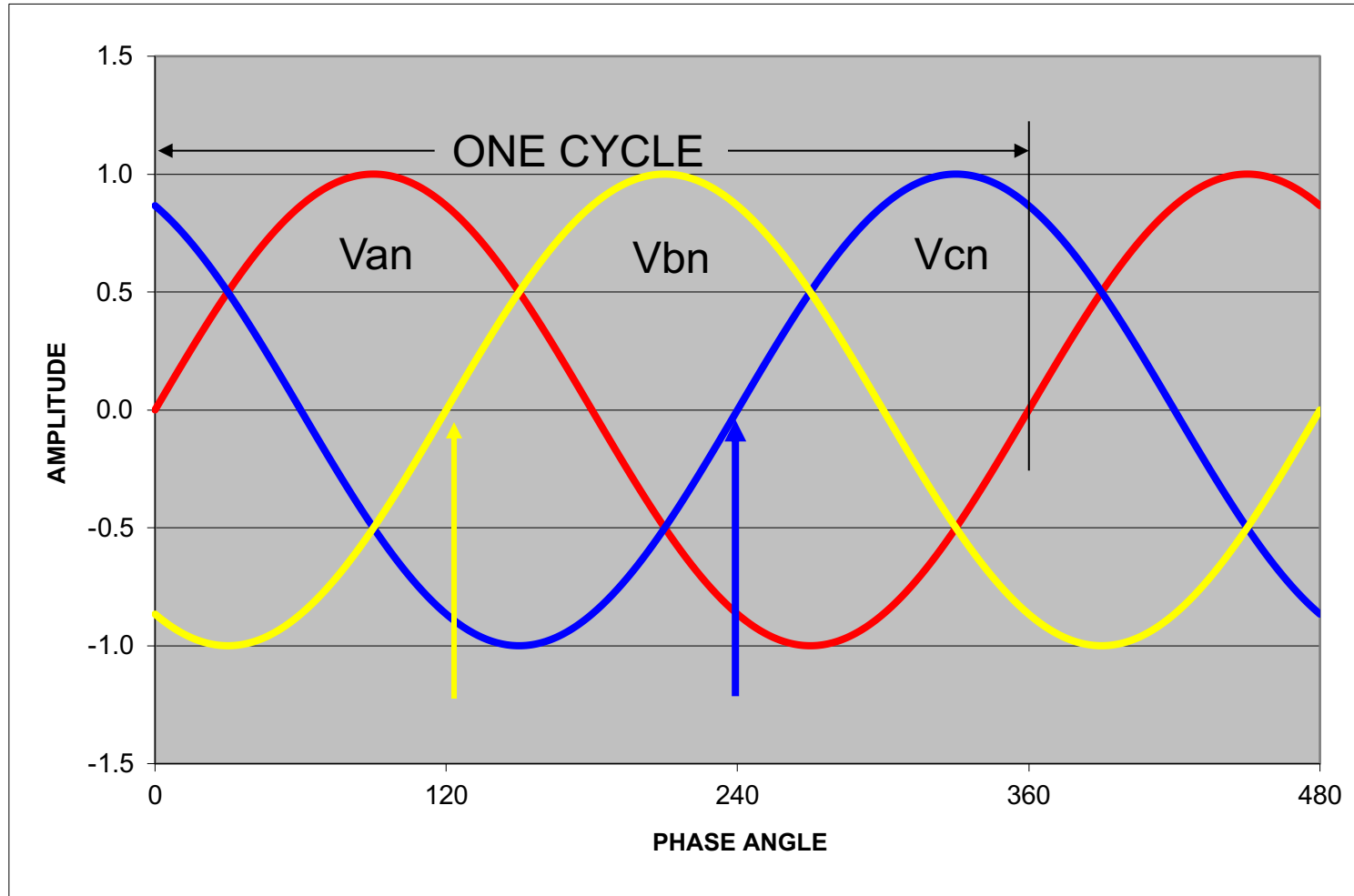
# Three Phase Theory

## Two Phases - Voltage Plot



# Three Phase Theory

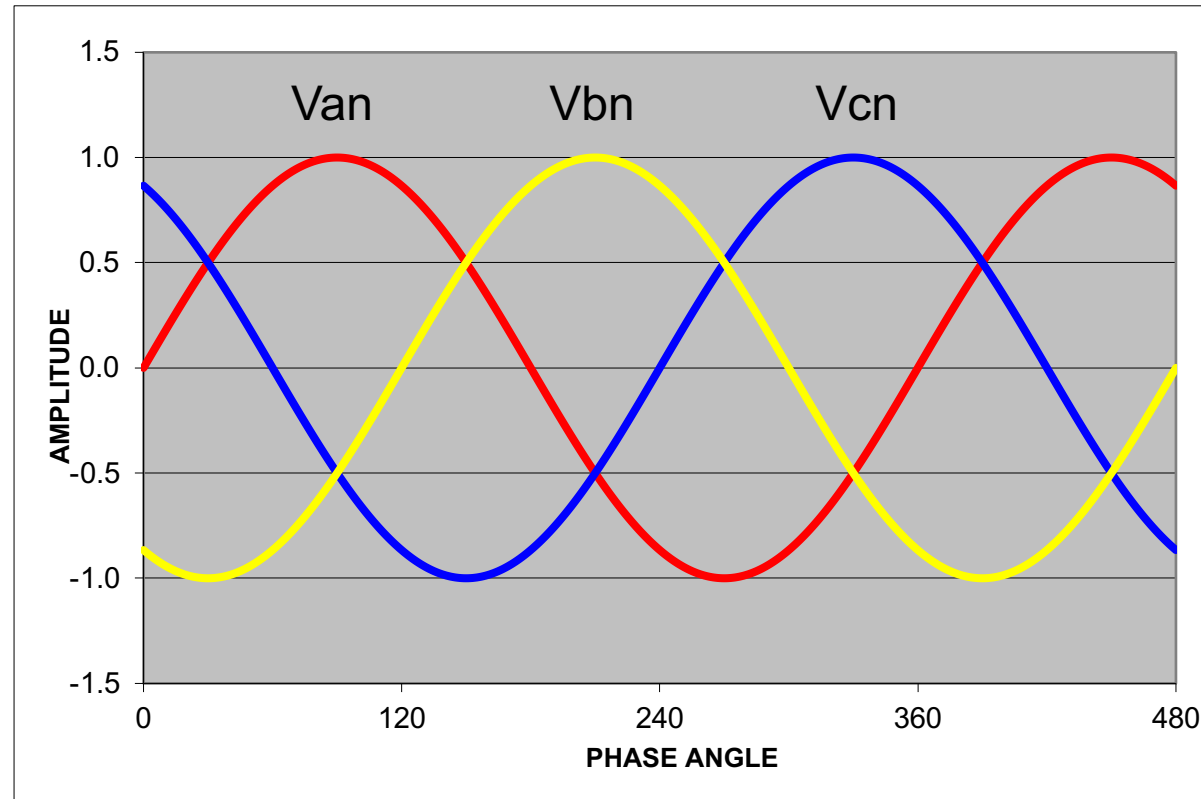
## Three Phase - Voltage Plot



# Three Phase Power At the Generator

Three voltage vectors  
each separated by  
 $120^\circ$ .

Peak voltages  
essentially equal.



**Most of what makes three phase systems seem complex is what we do to this simple picture in the delivery system and loads.**



# Three Phase Power

## Basic Concept – Phase Rotation

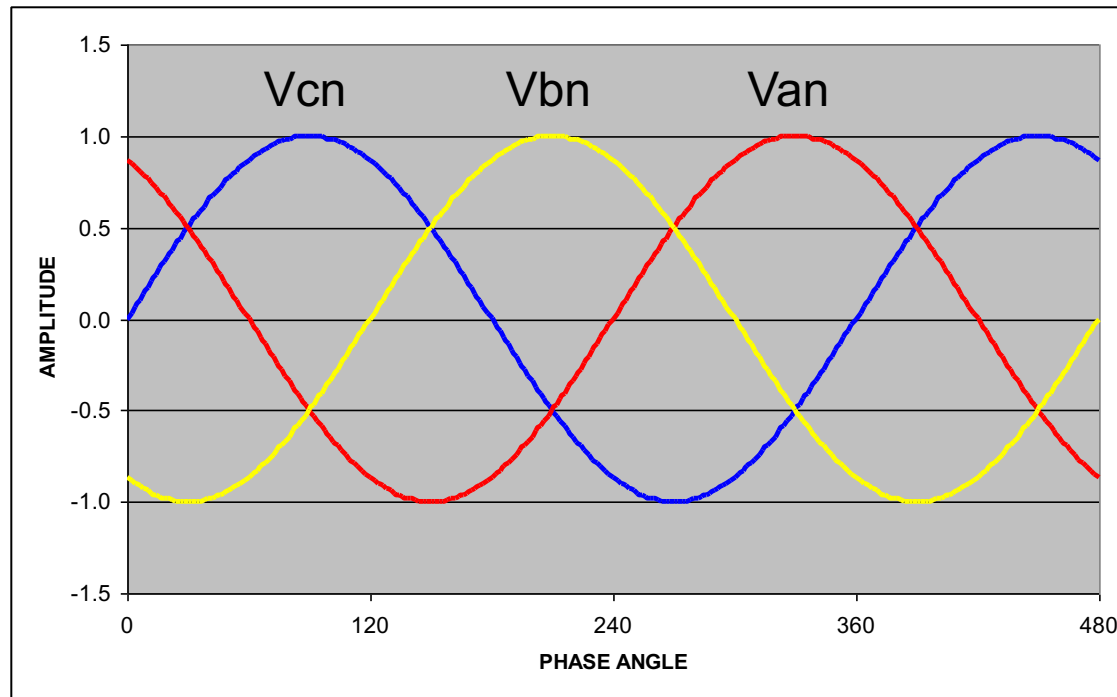
### Phase Rotation:

The order in which the phases reach peak voltage.

There are only two possible sequences:

A-B-C (previous slide)

C-B-A (this slide)

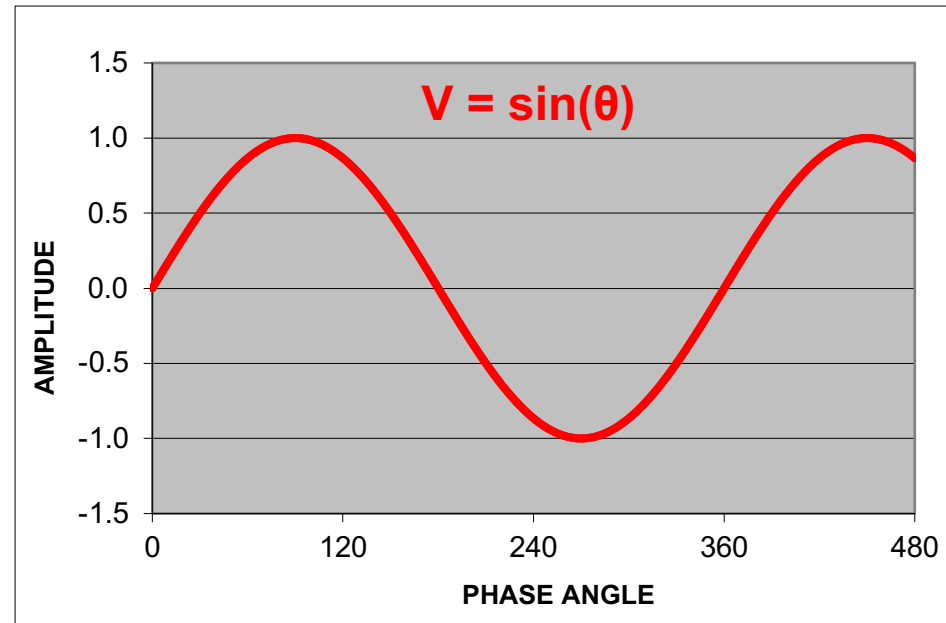
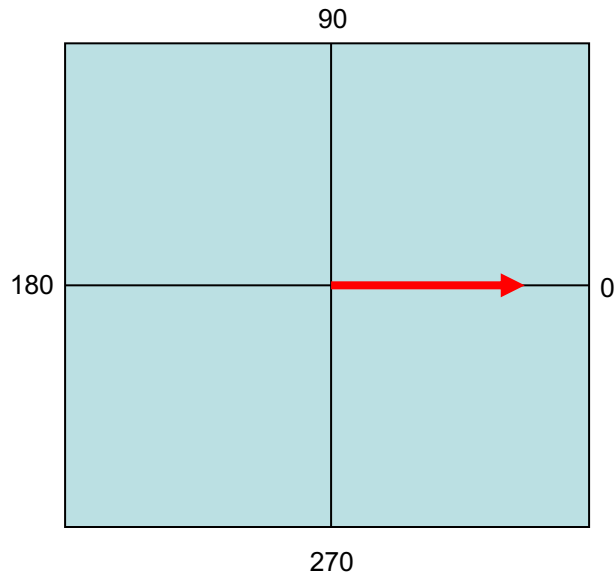


**Phase rotation is important because the direction of rotation of a three phase motor is determined by the phase order.**

# Three Phase Theory

## Phasors and Vector Notation

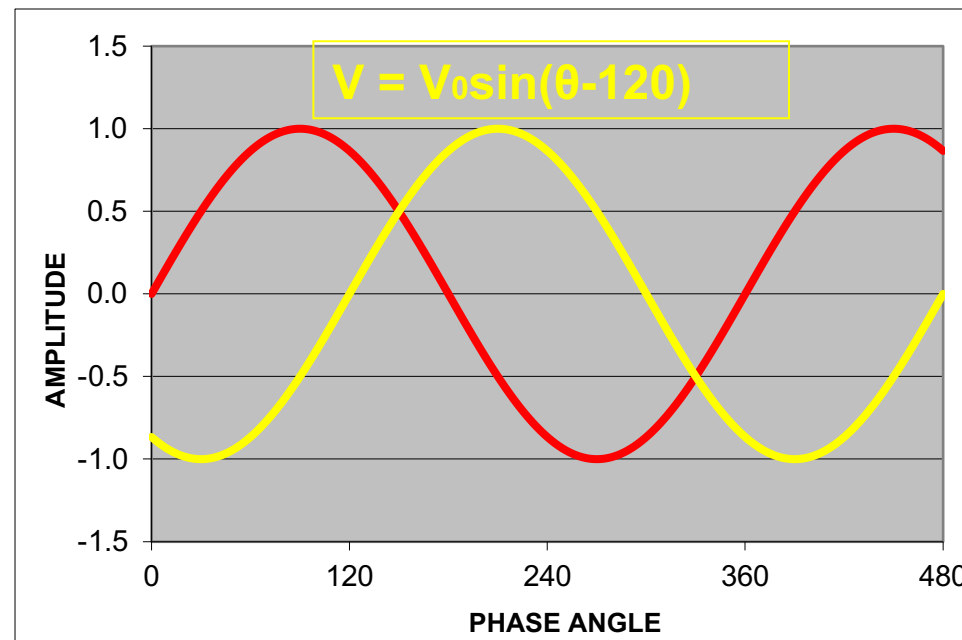
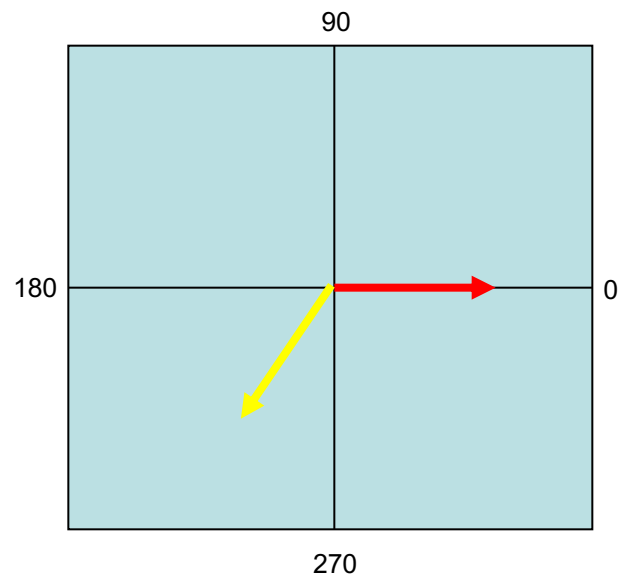
- Phasors are a graphical means of representing the amplitude and phase relationships of voltages and currents.



# Three Phase Power

## Phasors and Vector Notation

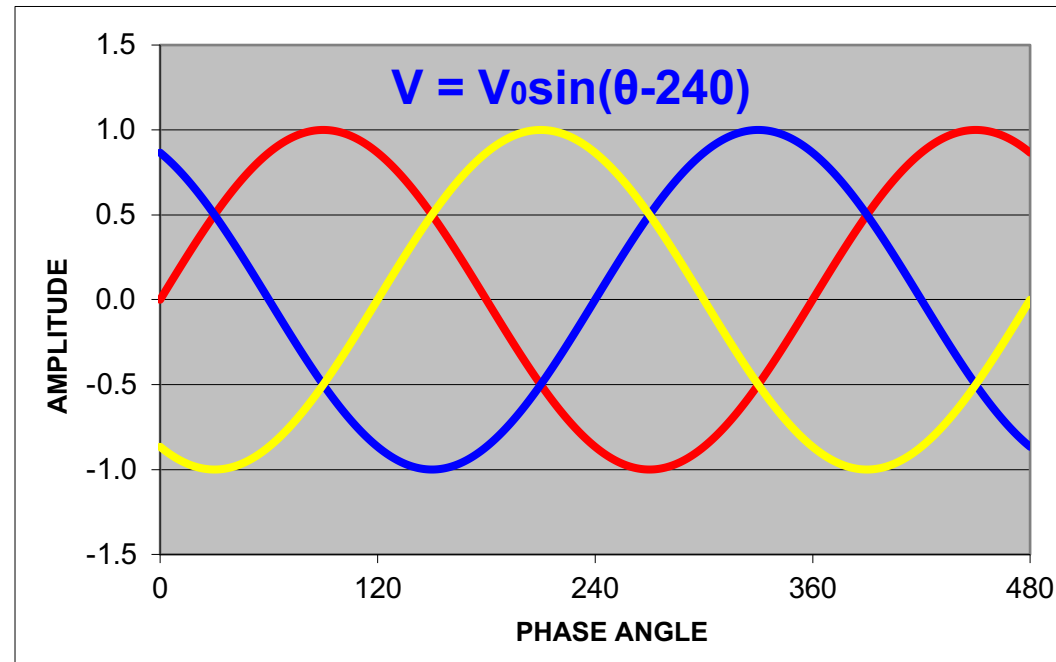
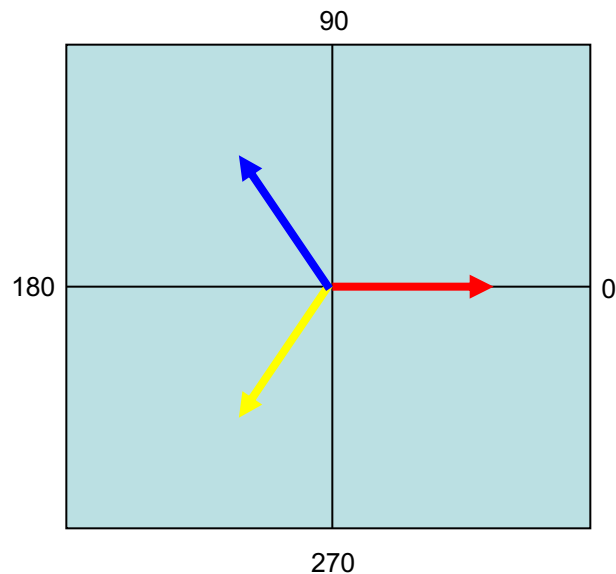
- As stated in the Handbook of Electricity Metering, by common consent, counterclockwise phase rotation has been chosen for general use in phasor diagrams.



# Three Phase Power

## Phasors and Vector Notation

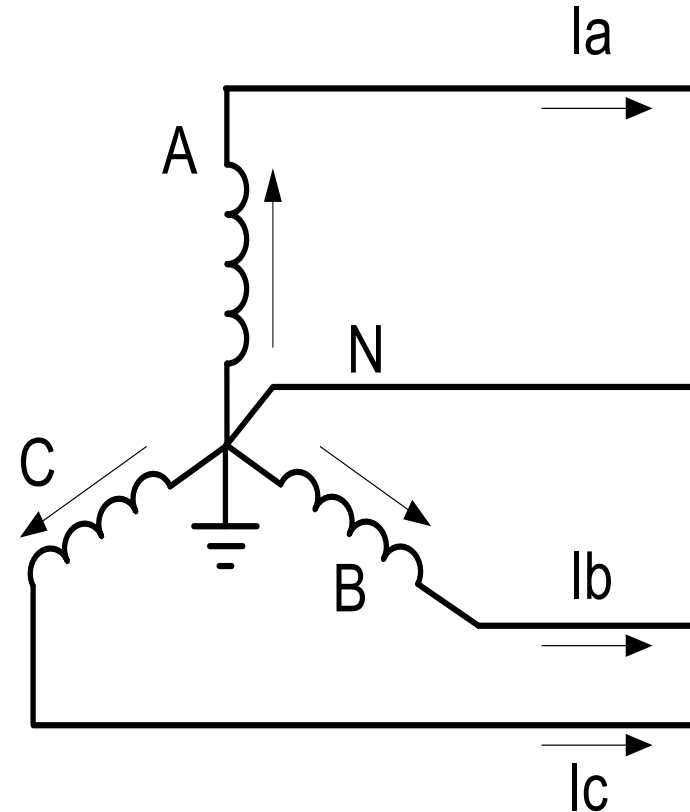
- The phasor diagram for a simple 3-phase system has three voltage phasors equally spaced at  $120^\circ$  intervals.
- Going clockwise the order is A – B – C.



# Three Phase Theory

## Symbols and Conventions

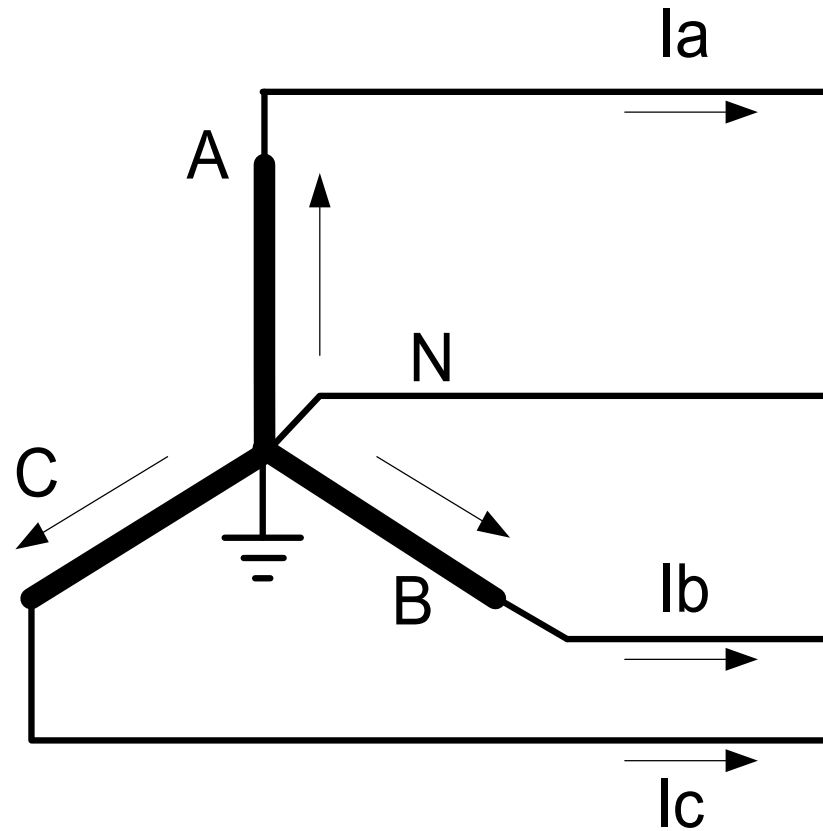
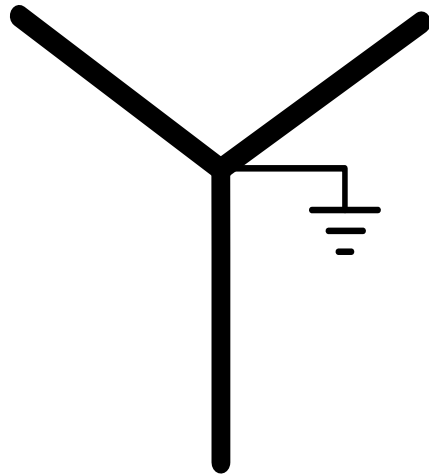
- Systems formed by interconnecting secondaries of 3 single phase transformers.
- Generally primaries are not shown unless details of actual transformer are being discussed.



# Three Phase Theory

## Symbols and Conventions

- Often even the coils are not shown but are replaced by simple line drawings

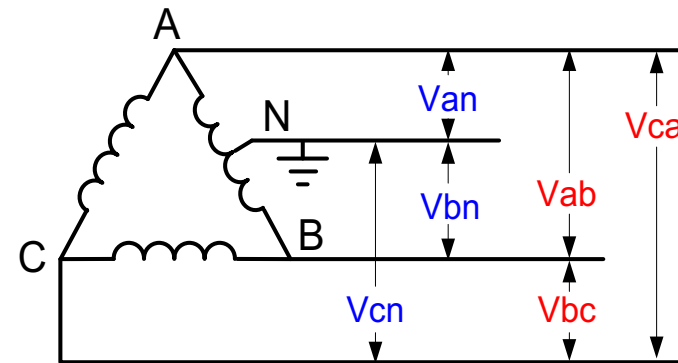


# Symbols and Conventions

## Labeling

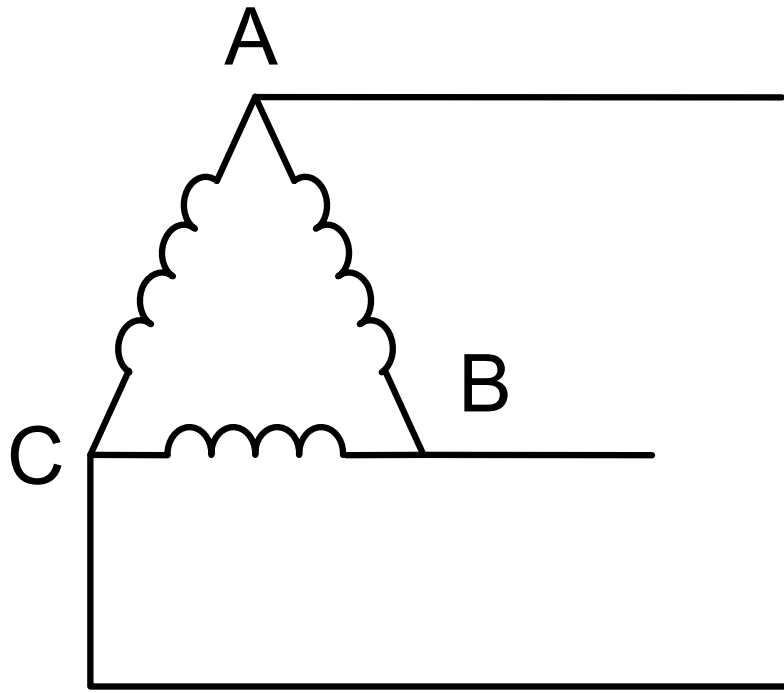
- Voltages are generally labeled  $V_a$ ,  $V_b$ ,  $V_c$ ,  $V_n$  for the three phases and neutral
- This can be confusing in complex cases.
- The recommended approach is to use two subscripts so the two points between which the voltage is measured are unambiguous.

$V_{ab}$  means voltage at “a” as measured relative to “b”.

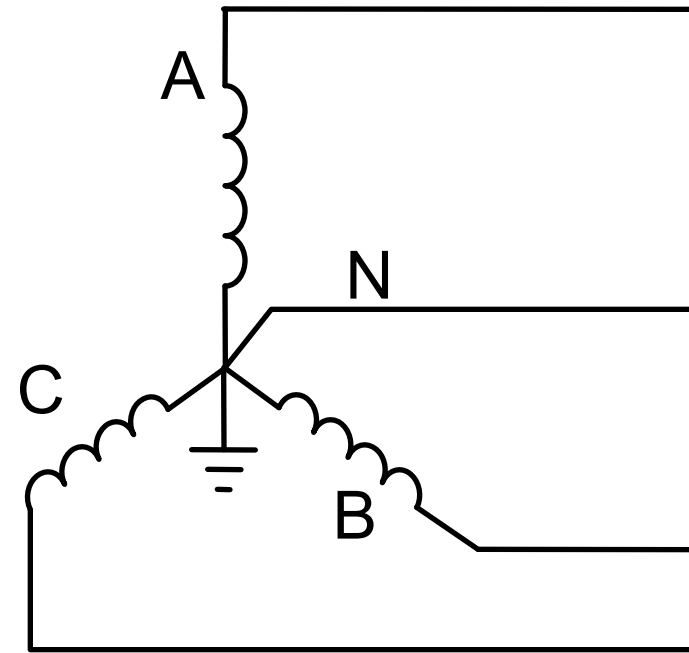


# Three Phase Transformers

## Delta vs Wye



Delta



Wye



# Three Phase Transformers

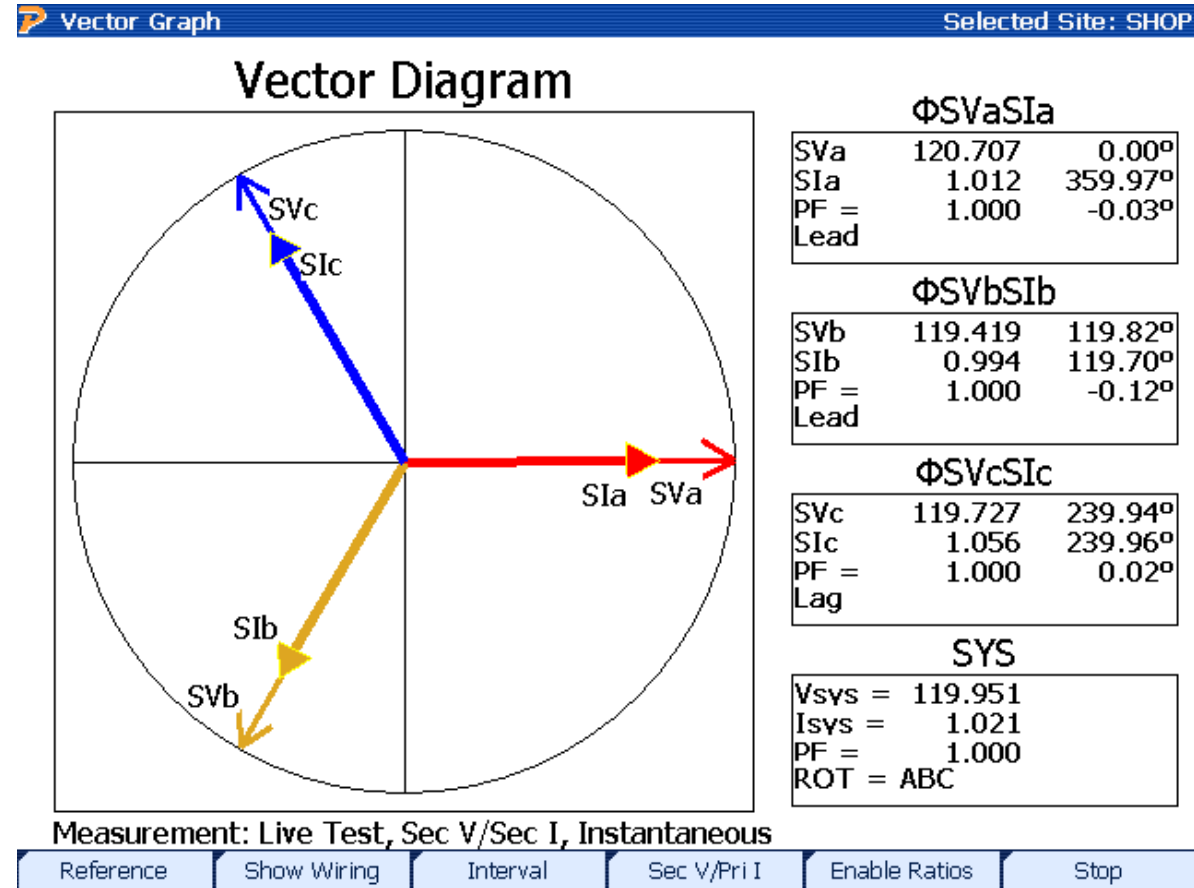
## Delta vs Wye

- Delta is commonly used for power transmission as it only requires three lines
- Delta is better for a balanced load like a motor and has greater reliability if a winding failure occurs
- Wye offers two voltages – line to neutral and line to line
- Wye is used when a single phase load is required

# 3 Phase, 4-Wire "Y" Service

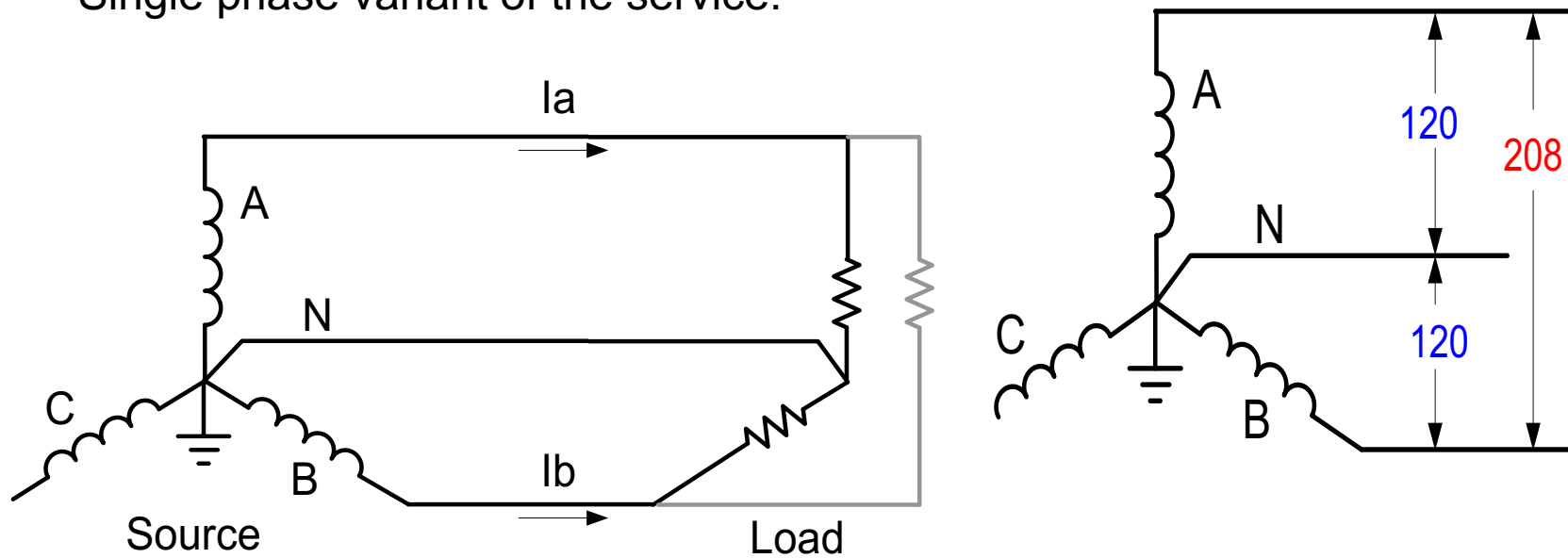
## 0° = Unity Power Factor

- Three Voltage Phasors
- 120° Apart
- Three Current Phasors
- Aligned with Voltage at PF=1



# 2 Phase, 3-Wire “Y” Service “Network Connection”

Single phase variant of the service.



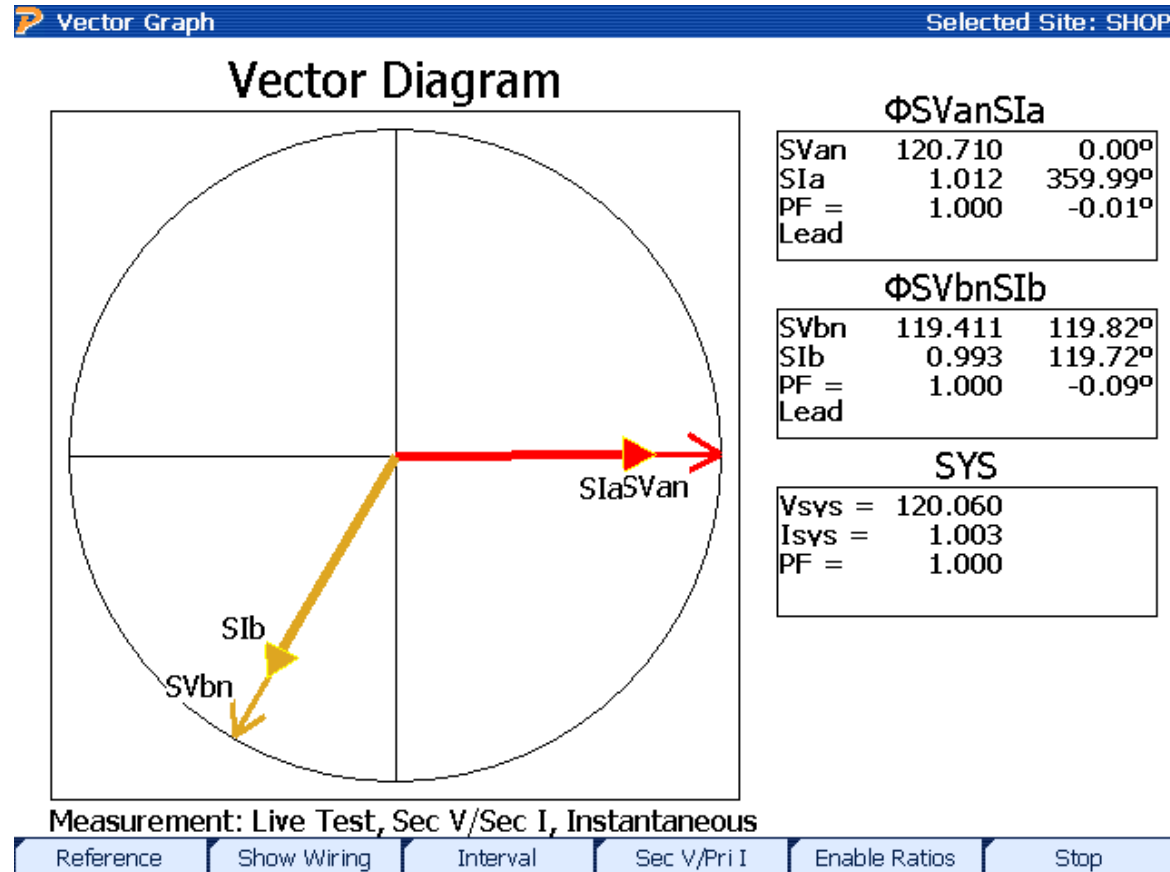
Two voltage sources with their returns connected to a common point.

Provides 208 rather than 240 volts across “high side” wires.

$$V_{AB} = \sqrt{3}V_{AN}$$

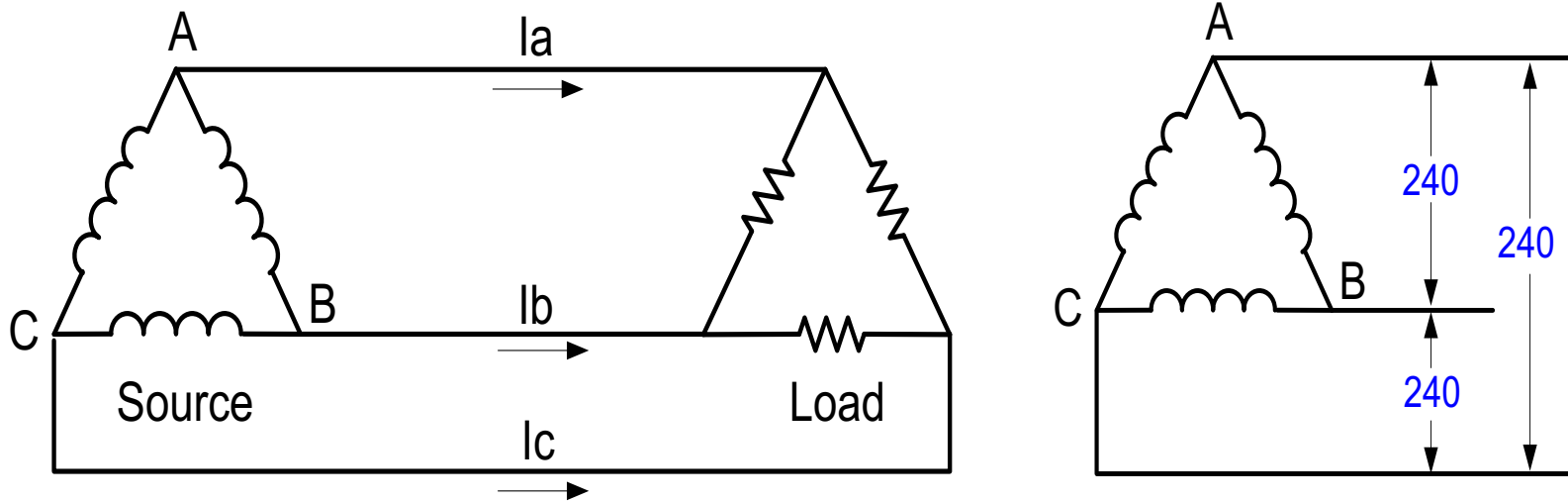
# 2 Phase, 3-Wire “Network” Service

- Two Voltage Phasors
- 120° Apart
- Two Current Phasors
- Aligned with Voltage at PF=1



# 3 Phase, 3-Wire Delta Service

Common service type for industrial customers. This service has NO neutral.

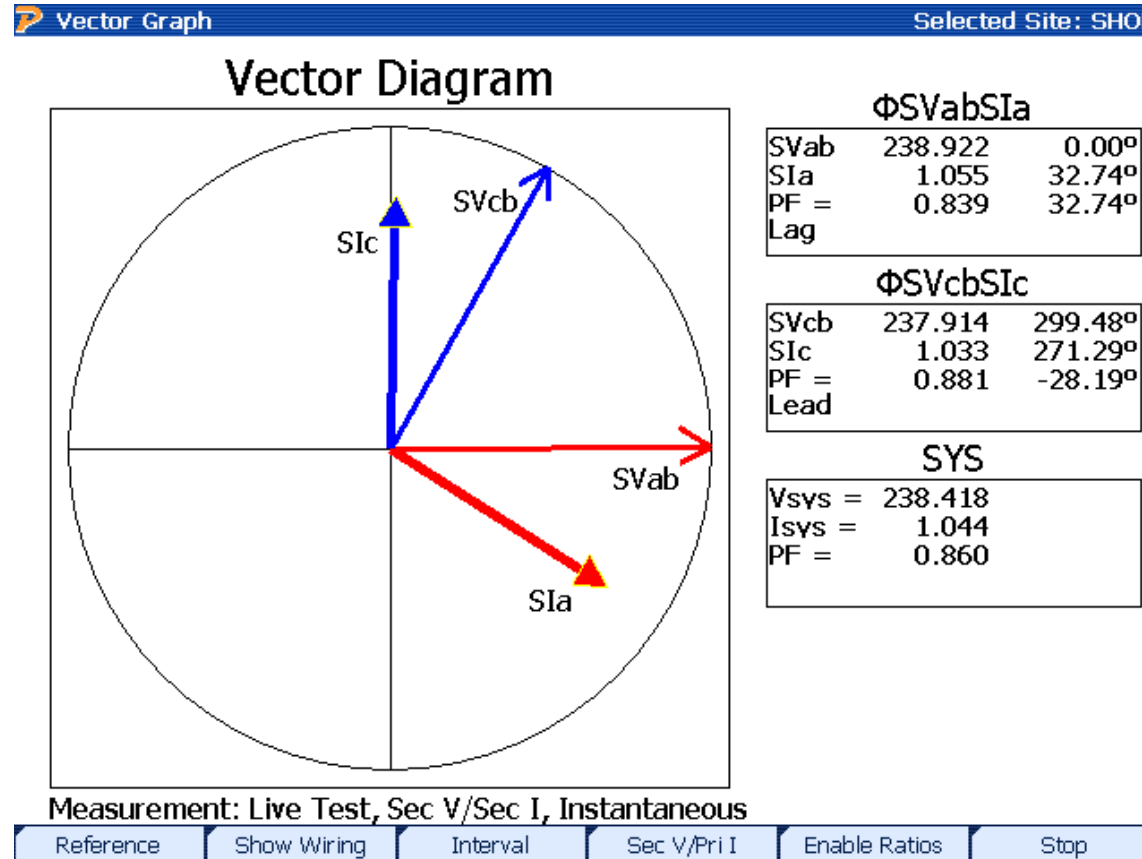


- Voltages normally measured relative to phase B.
- Voltage and current vectors do not align.
- Service is provided even when a phase is grounded.

# 3 Phase, 3-Wire Delta Service

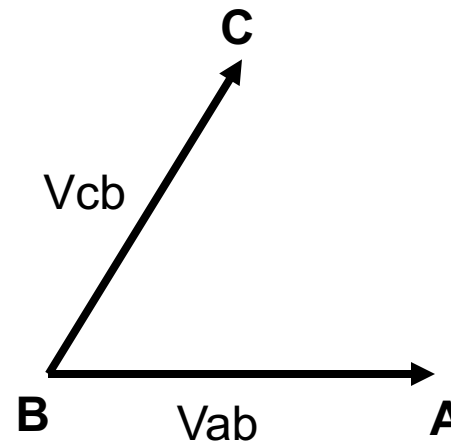
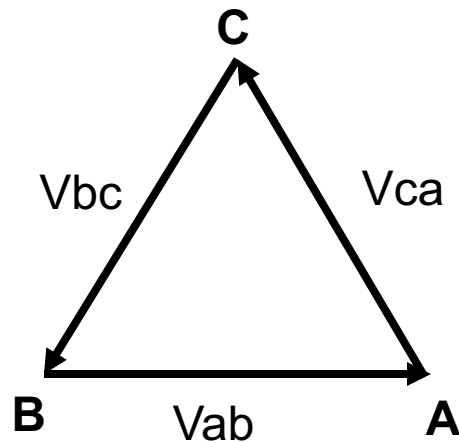
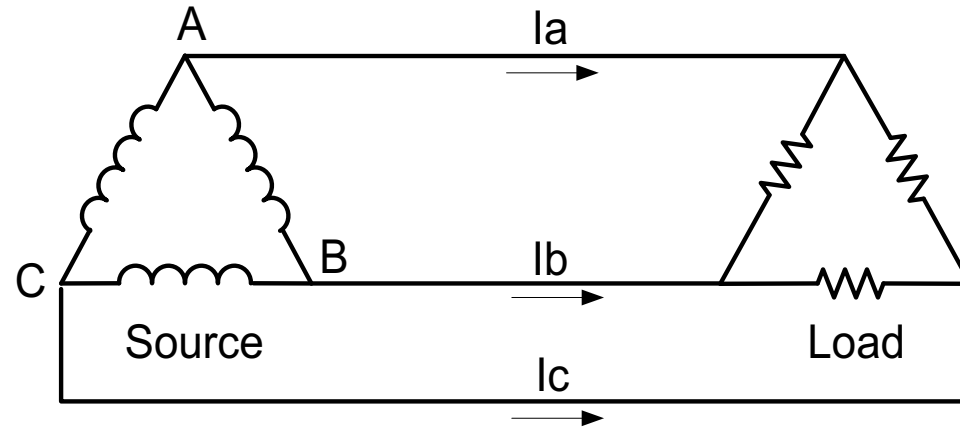
## Resistive Loads

- Two Voltage Phasors
- 60° Apart
- Two Current Phasors
- For a resistive load one current leads by 30° while the other lags by 30°



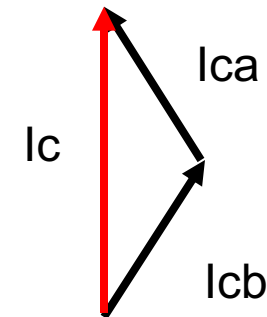
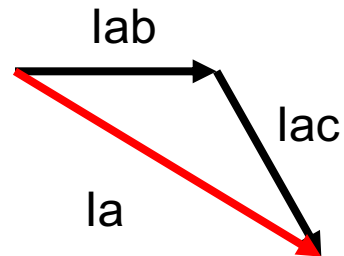
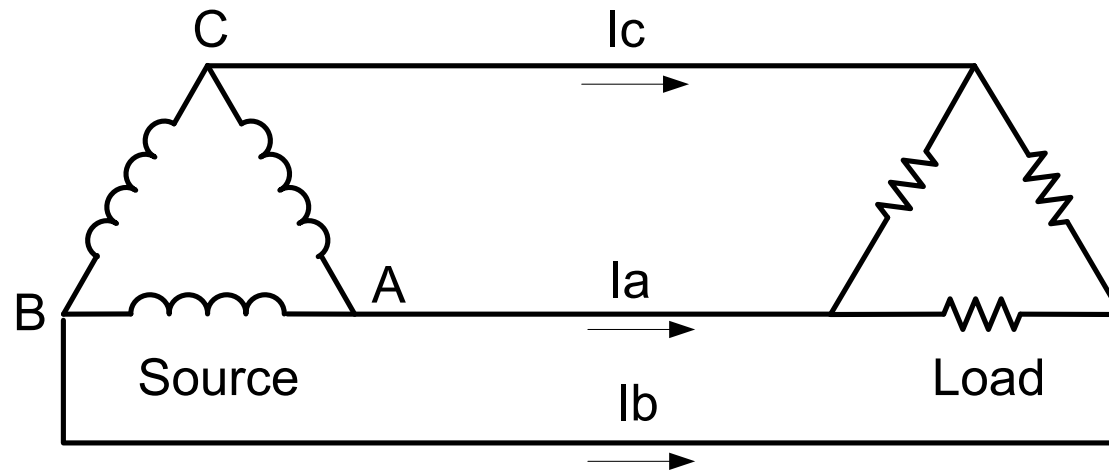
# 3 Phase, 3-Wire Delta Service

## Understanding the Diagram



# 3 Phase, 3-Wire Delta Service

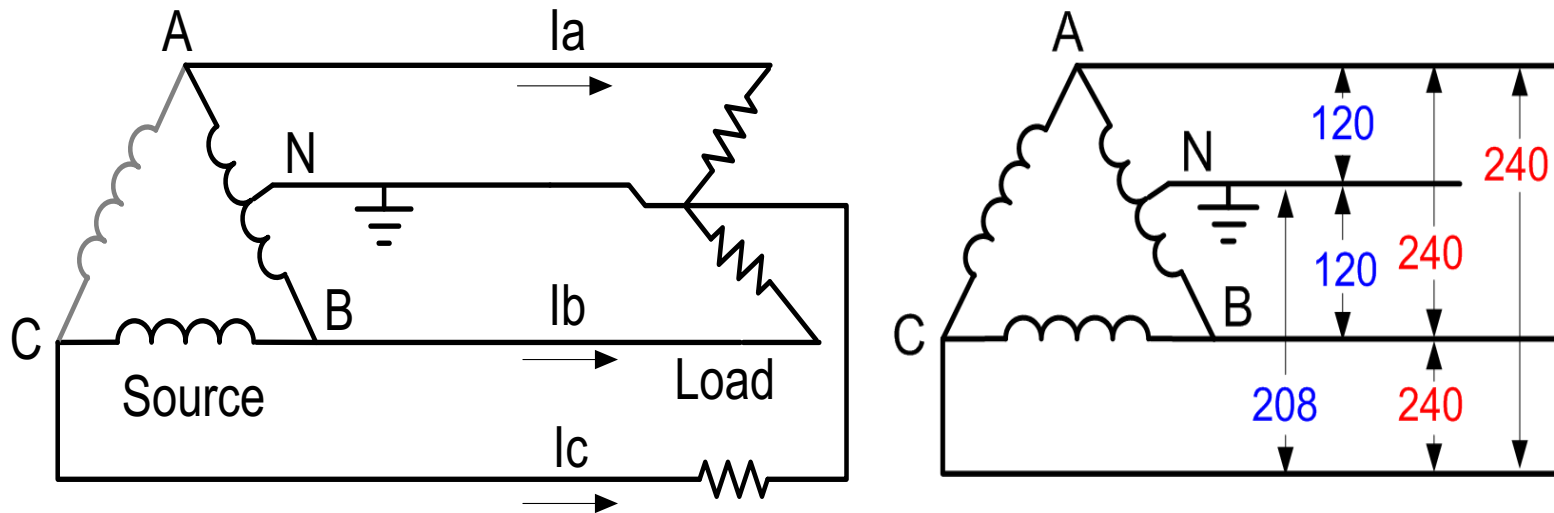
## Understanding the Diagram





# 3 Phase, 4-Wire Delta Service

Common service type for industrial customers. Provides a residential like 120/240 service (lighting service) single phase 208 (high side) and even 3 phase 240 V.

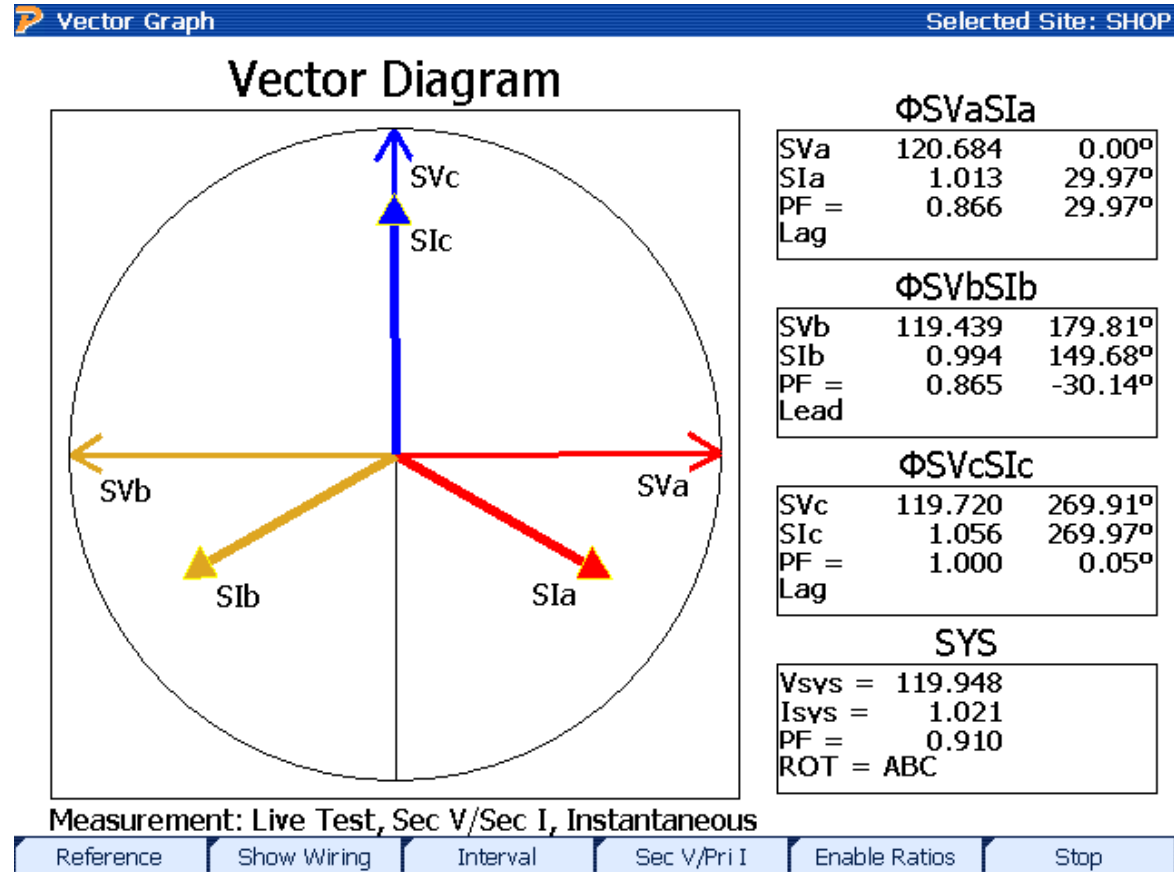


- Voltage phasors form a “T” 90° apart
- Currents are at 120° spacing
- In 120/120/208 form only the “hot” (208) leg has its voltage and current vectors aligned.

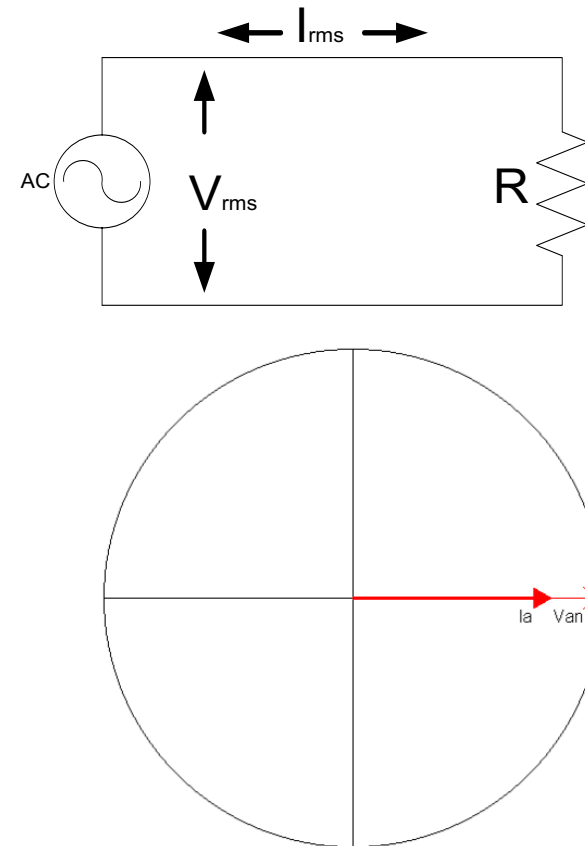
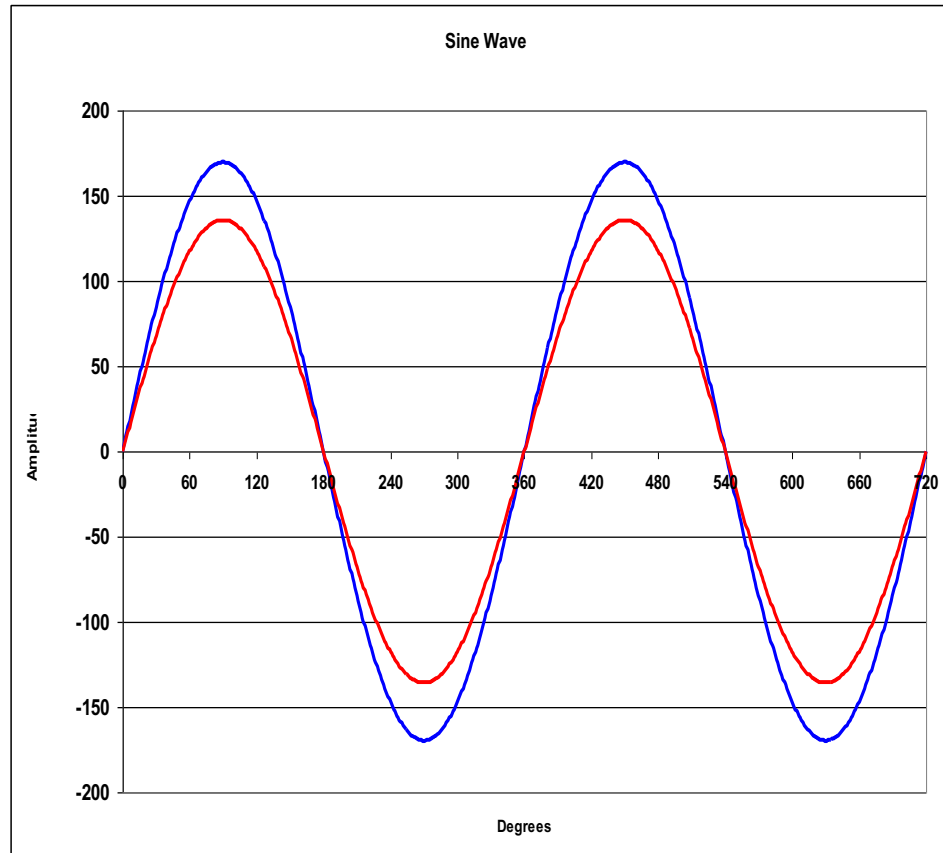
# 3 Phase, 4-Wire Delta Service

## Resistive Load

- Three Voltage Phasors
- 90° Apart
- Three Current Phasors
- 120° apart

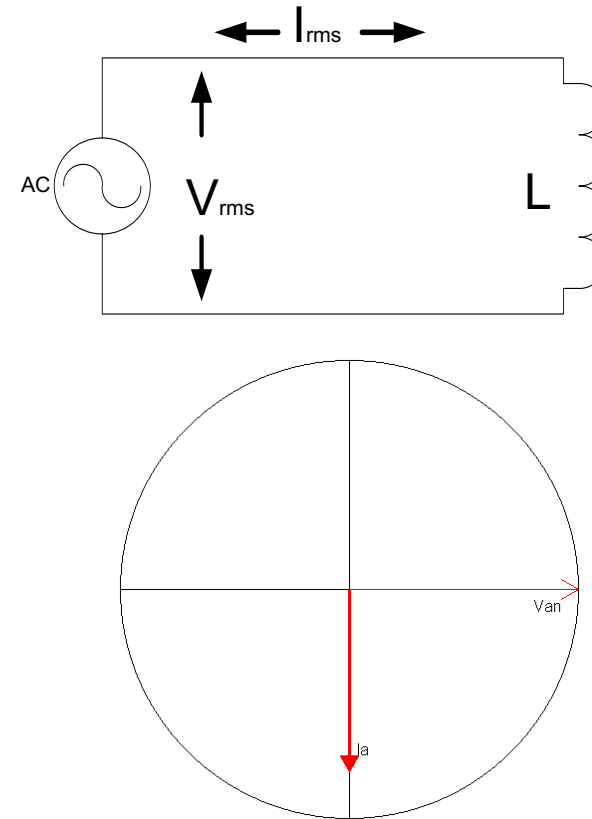
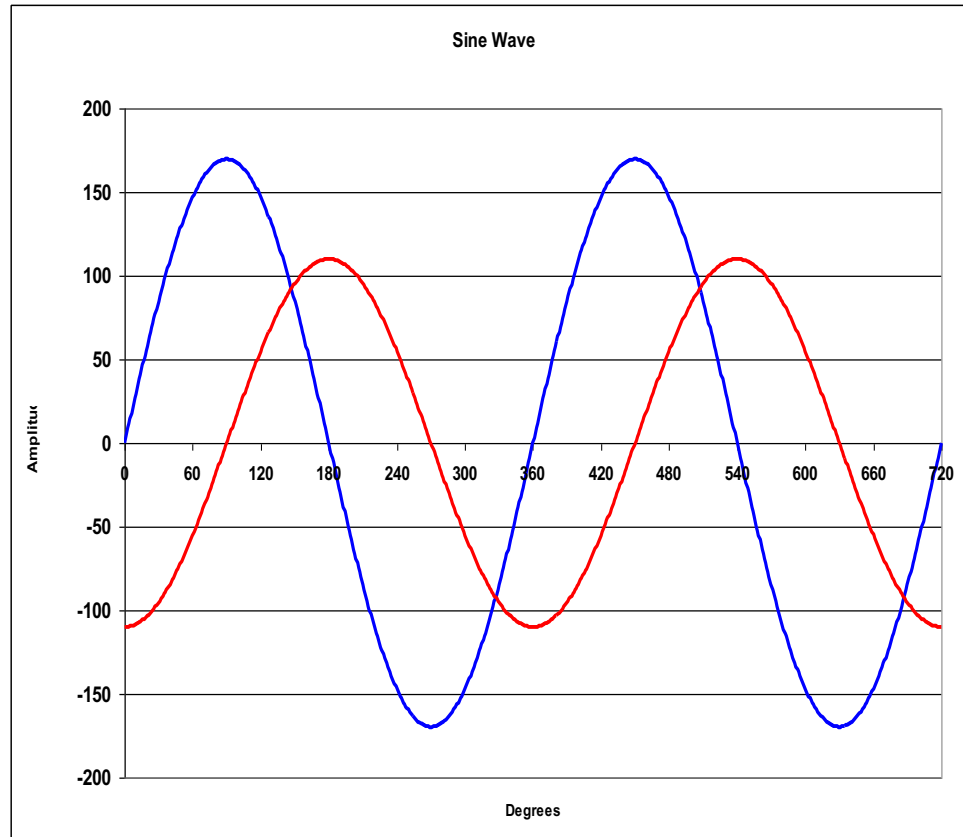


# AC Theory – Resistive Load



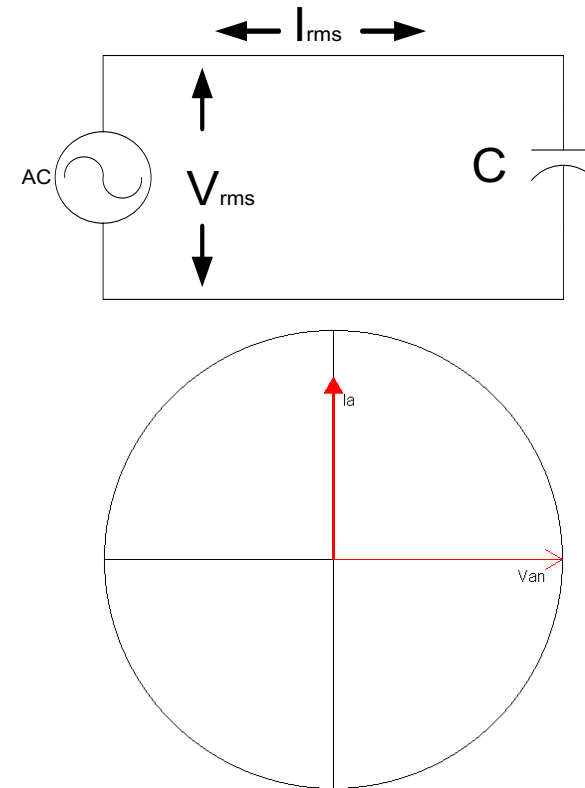
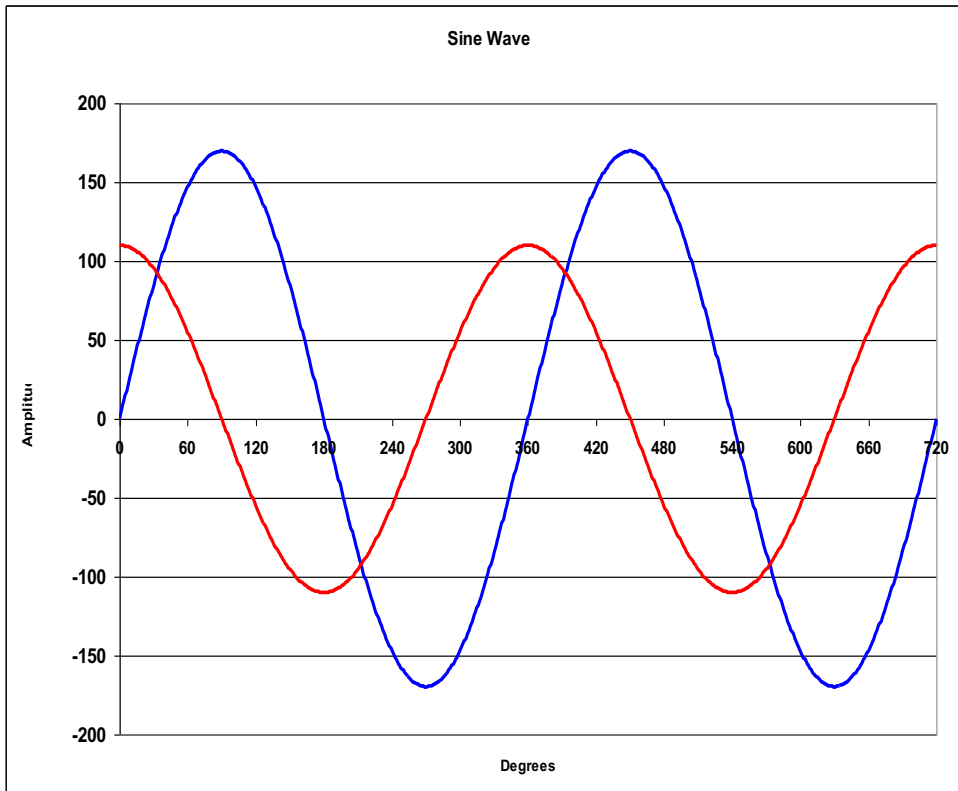
Resistors are measured in Ohms. When an AC voltage is applied to a resistor, the current is in phase. A resistive load is considered a “linear” load because when the voltage is sinusoidal the current is also sinusoidal.

# AC Theory – Inductive Load



Inductors are measured in Henries. When an AC voltage is applied to an inductor, the current is 90 degrees out of phase. We say the current “lags” the voltage. A inductive load is considered a “linear” load because when the voltage is sinusoidal the current is also sinusoidal.

# AC Theory – Capacitive Load



Capacitors are measured in Farads. When an AC voltage is applied to a capacitor, the current is 90 degrees out of phase. We say the current “leads” the voltage. A capacitive load is considered a “linear” load because when the voltage is sinusoidal the current is sinusoidal.

# AC Theory – Power

- Power is defined as  $P = VI$
- Since the voltage and current at every point in time for an AC signal is different, we have to distinguish between instantaneous power and average power. Generally when we say “power” we mean average power.
- Average power is only defined over an integral number of cycles.

# Time Out for Trig

(Right Triangles)

The Right Triangle:

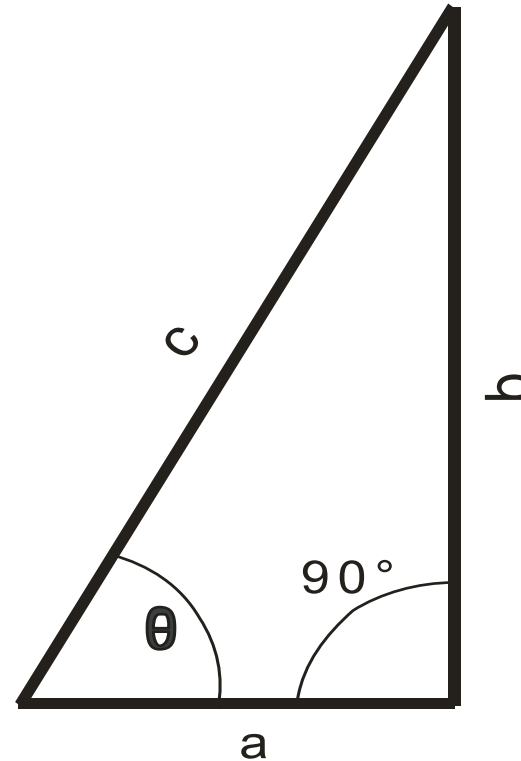
The Pythagorean theory

$$c^2 = a^2 + b^2$$

$$\text{Sin}(\theta) = \frac{b}{c}$$

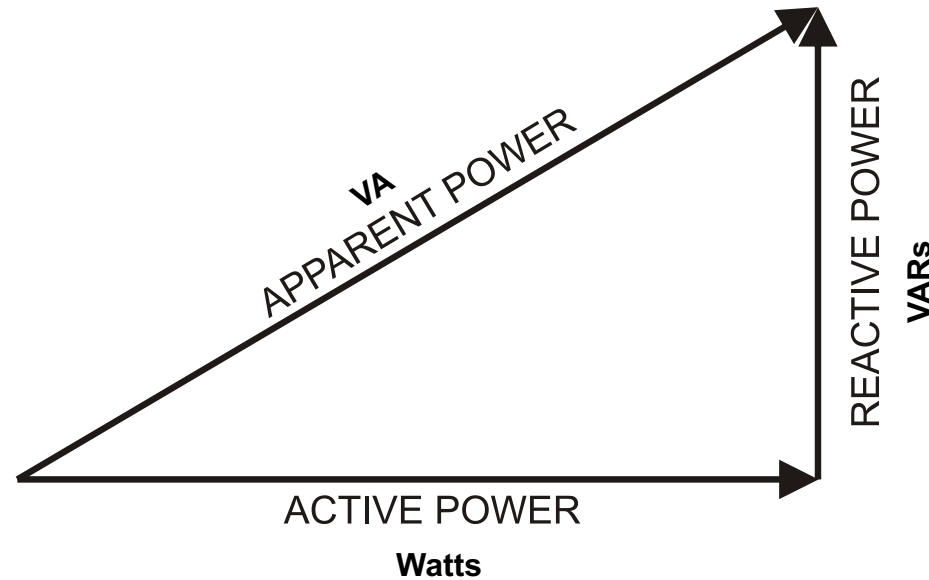
$$\text{Cos}(\theta) = \frac{a}{c}$$

$$\text{Tan}(\theta) = \frac{b}{a}$$



# AC Theory – Power Triangle

(Sinusoidal Waveforms)



If  $V = \sin(\omega t)$  and  $I = \sin(\omega t - \theta)$  (the load is linear)  
then

$$\text{Active Power} = VI \cos(\theta) \quad \text{Watts}$$

$$\text{Reactive Power} = VI \sin(\theta) \quad \text{VARs}$$

$$\text{Apparent Power} = VI \quad \text{VA}$$

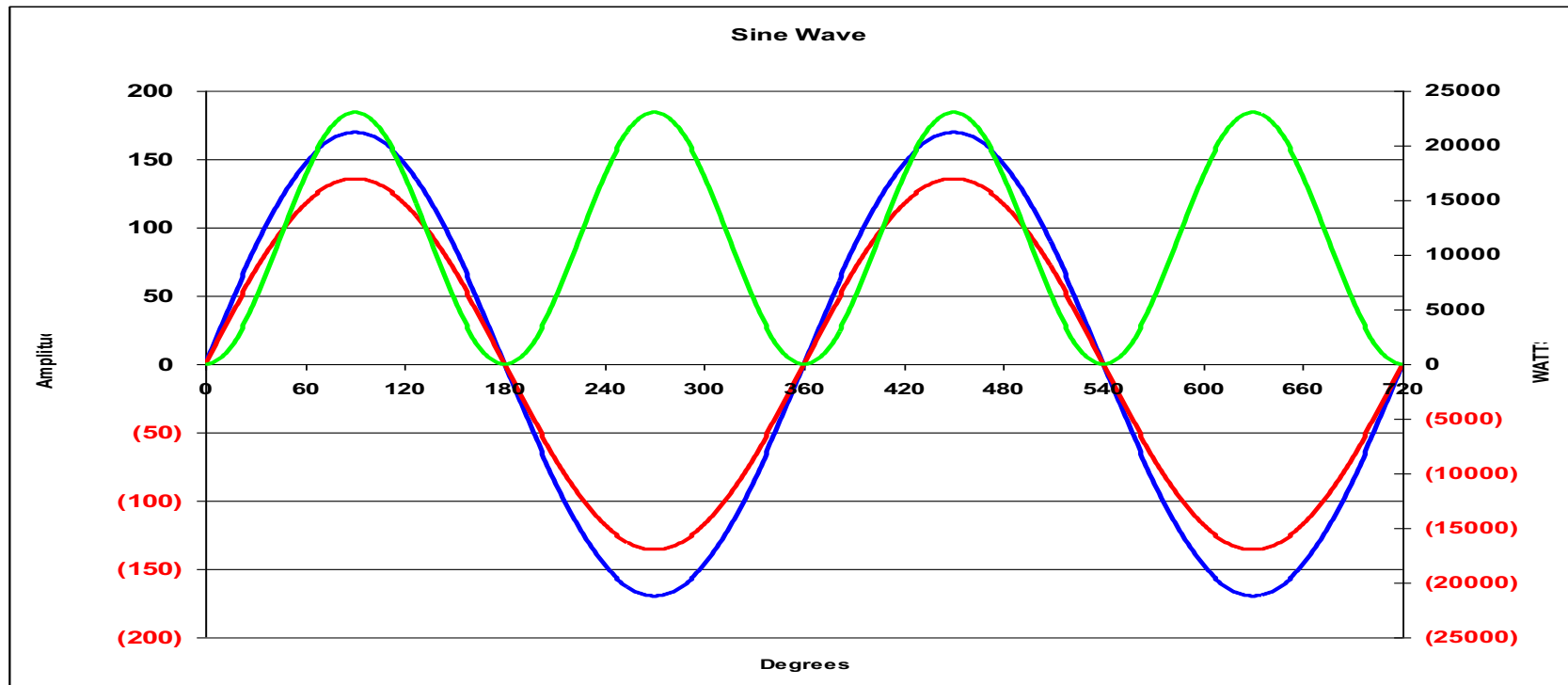
$$\text{Power Factor} = \frac{\text{Active}}{\text{Apparent}} = \cos(\theta)$$



# AC Theory

## Instantaneous Power

For a resistive load:  $p = vi = 2VI\text{Sin}^2(\omega t) = VI(1 - \text{Cos}(2\omega t))$



$$V = 120\sqrt{2}\text{Sin}(2\pi ft)$$

$$I = 96\sqrt{2}\text{Sin}(2\pi ft)$$

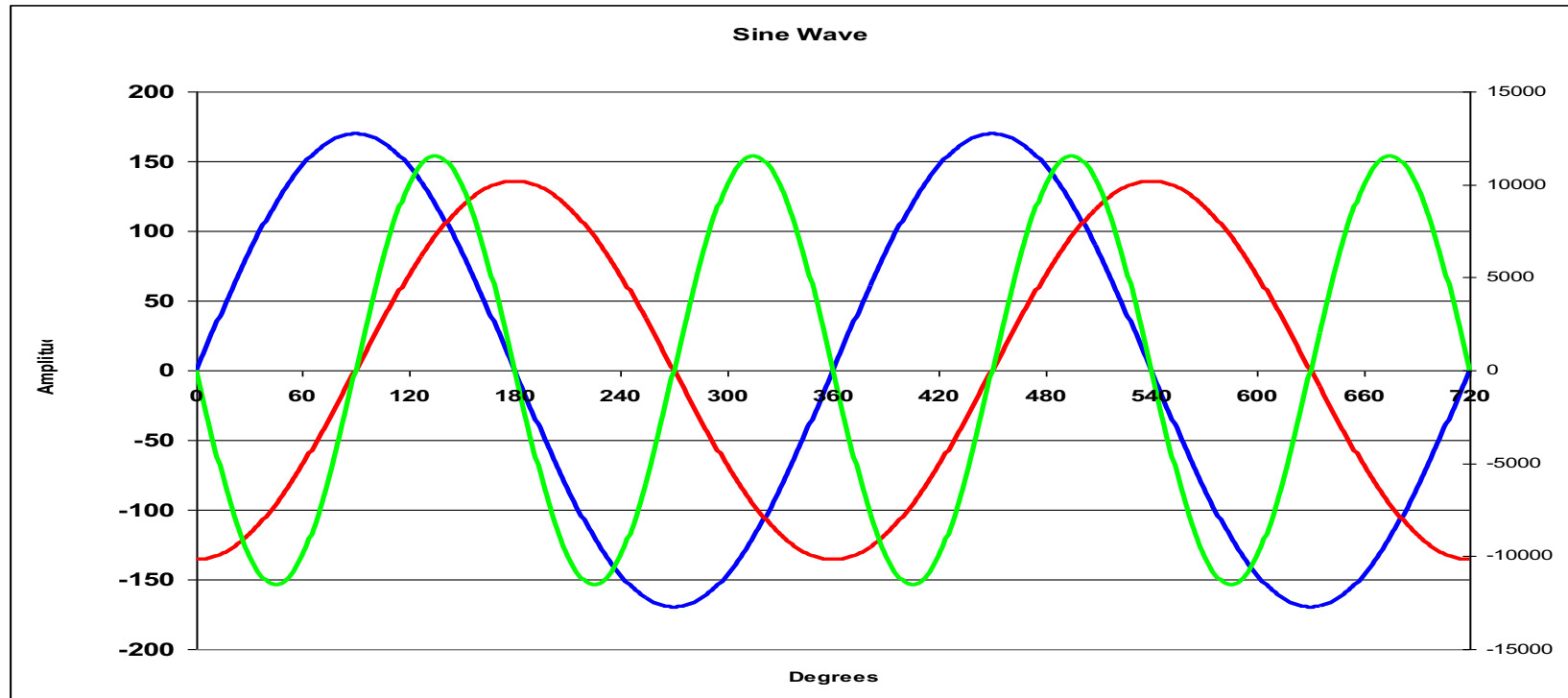
$$P = 23040\text{Sin}^2(2\pi ft)$$

$$P = 11520 \text{ Watts}$$

# AC Theory

## Instantaneous Power

For an inductive load:  $p = vi = 2VI\sin(\omega t)\sin(\omega t - 90) = -VI\sin(2\omega t)$



$$V = 120\sqrt{2}\sin(2\pi ft)$$

$$I = 96\sqrt{2}\sin(2\pi ft - 90)$$

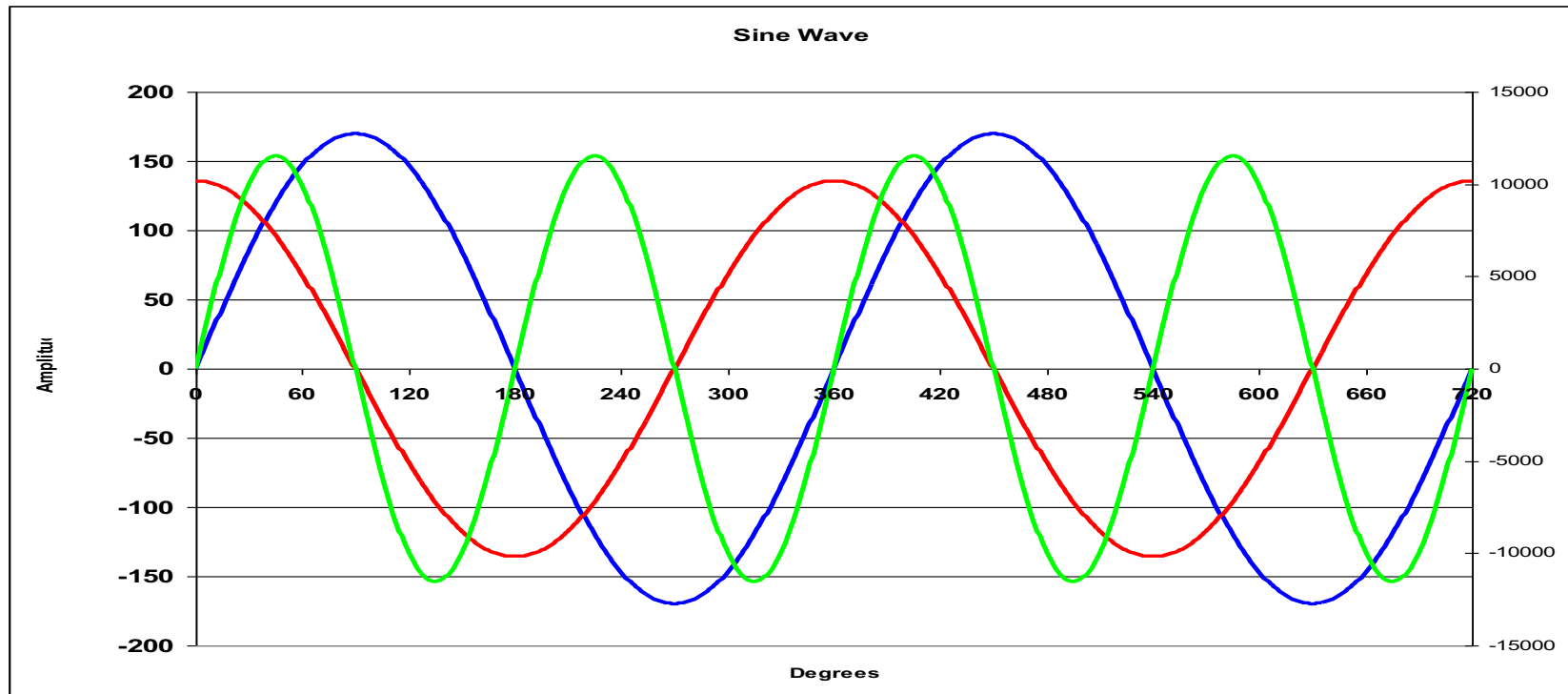
$$P = -11520\sin(2\pi ft)$$

$P = 0$  Watts

# AC Theory

## Instantaneous Power

For a capacitive load:  $p = vi = 2VI\sin(\omega t)\sin(\omega t + 90) = VI\sin(2\omega t)$



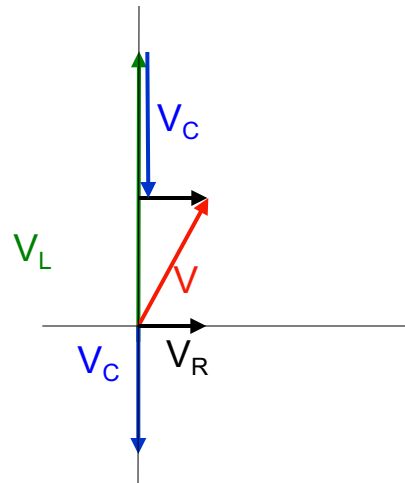
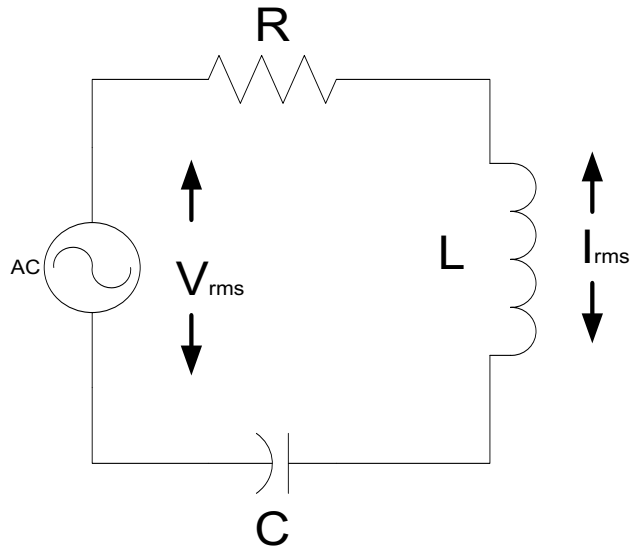
$$V = 120\sqrt{2}\sin(2\pi ft)$$

$$I = 96\sqrt{2}\sin(2\pi ft + 90)$$

$$P = 11520\sin(2\pi ft)$$

P = 0 Watts

# AC Theory – Complex Circuits



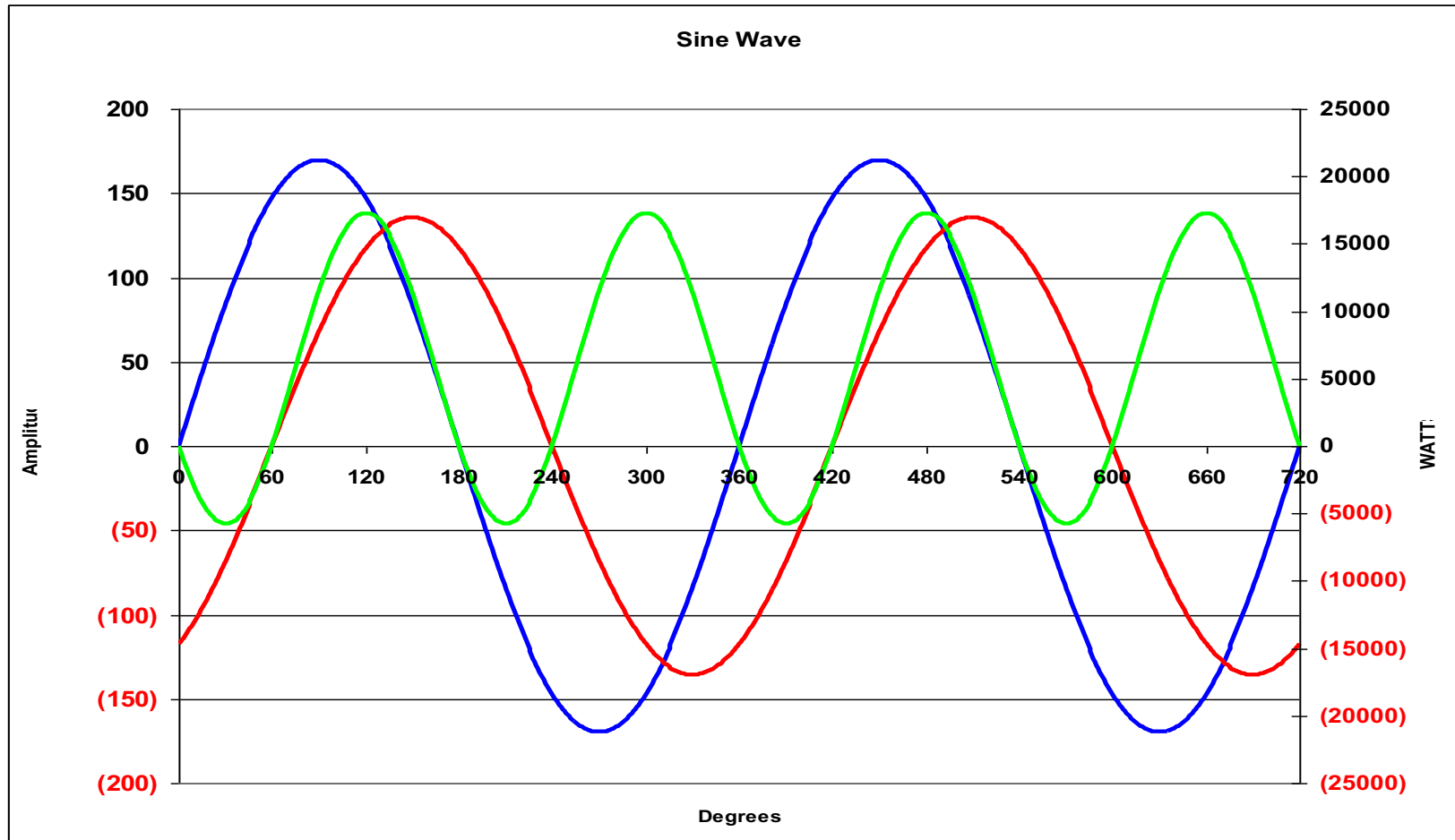
Amplitude (Current)

$$I = \frac{V}{\sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}}$$

Phase (Current)

$$\varphi = \text{ArcTan} \left[ \frac{\left(\omega L - \frac{1}{\omega C}\right)}{R} \right]$$

# AC Theory – Instantaneous Power



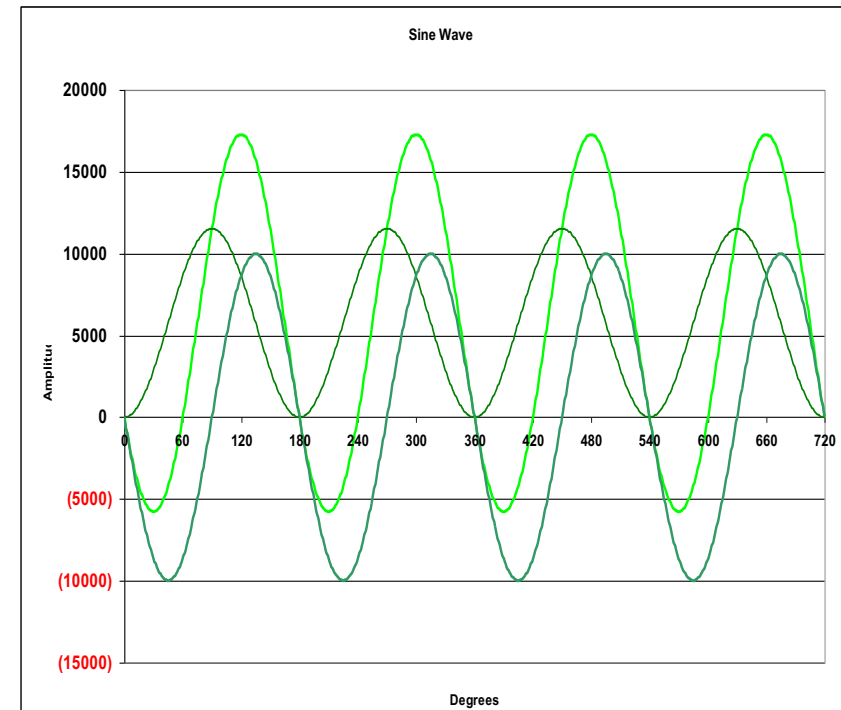
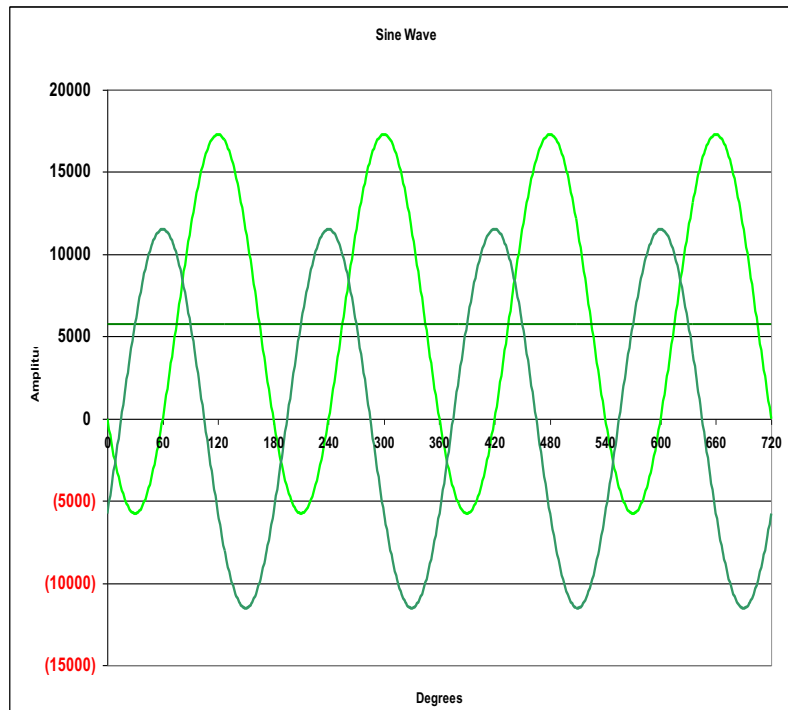
$$V = 120\sqrt{2}\sin(2\pi ft)$$

$$I = 96\sqrt{2}\sin(2\pi ft - 60)$$

$$P = VI = 23040(\cos(60^\circ) + \cos(4\pi ft - 60^\circ)) = 19953 - 23040\cos(4\pi ft - 60^\circ)$$

# AC Theory – Instantaneous Power

- From IEEE1459 instantaneous power can be written in several forms:



Active Power

Reactive Power

$$p = VI \cos \theta - VI \cos(2\omega t - \theta) \quad p = VI \cos \theta [1 - \cos(2\omega t)] - VI \sin \theta \sin(2\omega t)$$

# Three Phase Power

## Blondel's Theorem

If energy be supplied to any system of conductors through  $N$  wires, the total power in the system is given by the algebraic sum of the readings of  $N$  wattmeters, so arranged that each of the  $N$  wires contains one current coil, the corresponding voltage coil being connected between that wire and some common point. If this common point is on one of the  $N$  wires, the measurement may be made by the use of  $N-1$  wattmeters.

# Three Phase Power

## Blondel's Theorem

- Simply – We can measure the power in a N wire system by measuring the power in N-1 conductors.
- For example, in a 4-wire, 3-phase system we need to measure the power in 3 circuits.

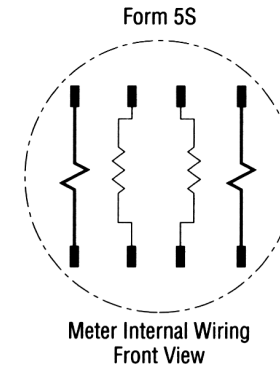
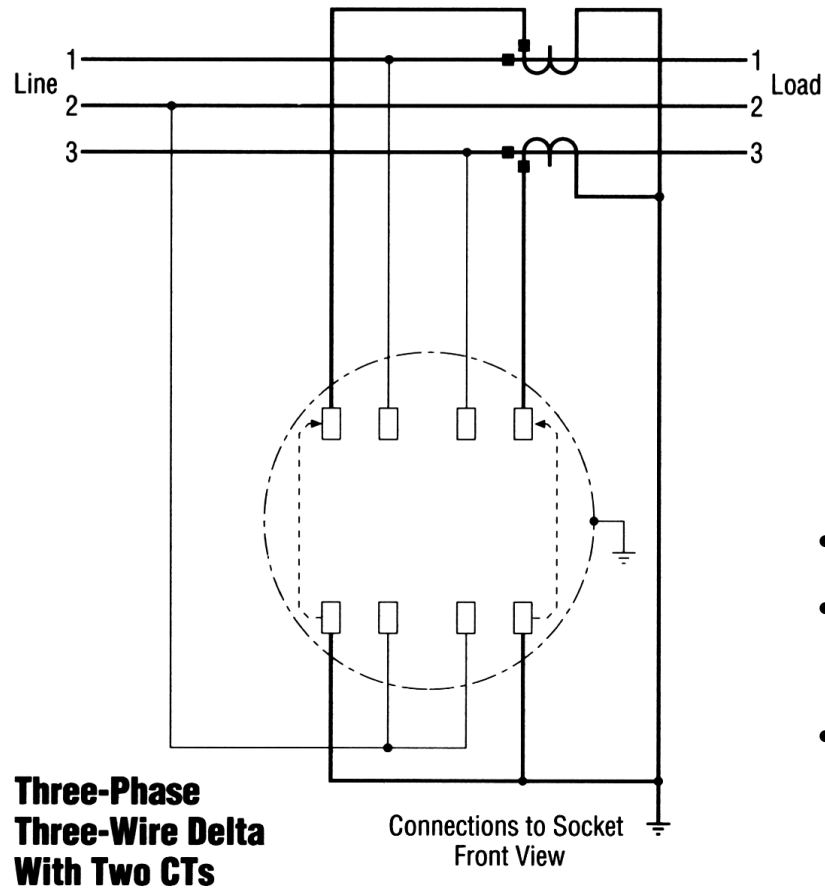


# Three Phase Power

## Blondel's Theorem

- If a meter installation meets Blondel's Theorem then we will get accurate power measurements under all circumstances.
- If a metering system does not meet Blondel's Theorem then we will only get accurate measurements if certain assumptions are met.

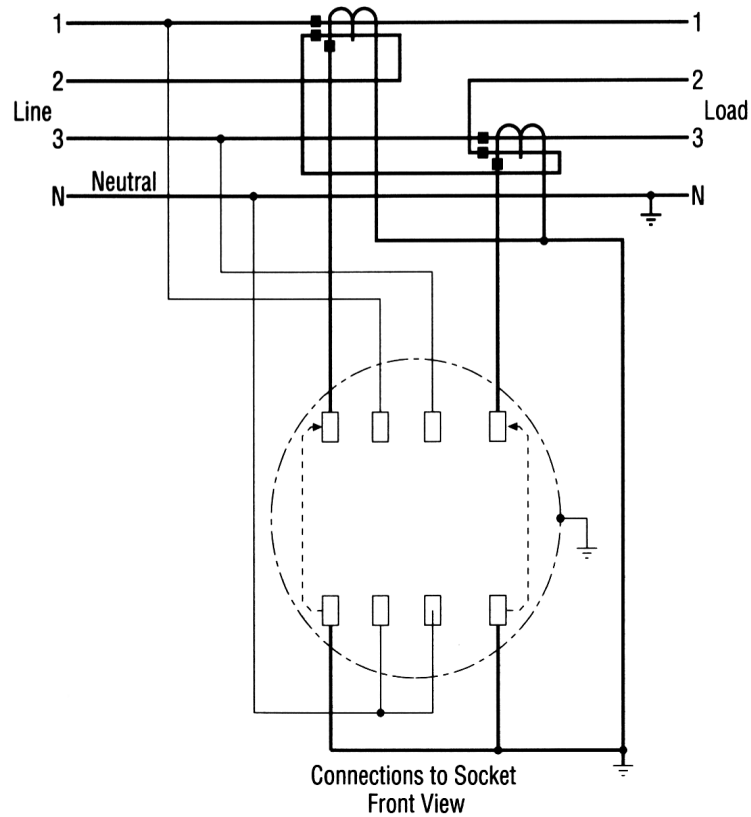
# Blondel's Theorem



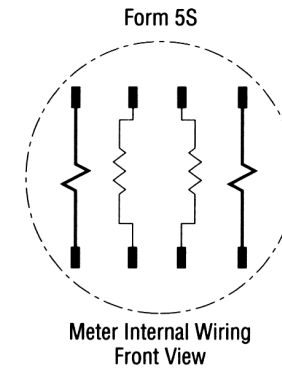
- Three wires
- Two voltage measurements with one side common to Line 2
- Current measurements on lines 1 & 3.

**This satisfies Blondel's Theorem.**

# Blondel's Theorem



**Three-Phase  
Four-Wire Wye  
With Two Equal-Ratio CTs**



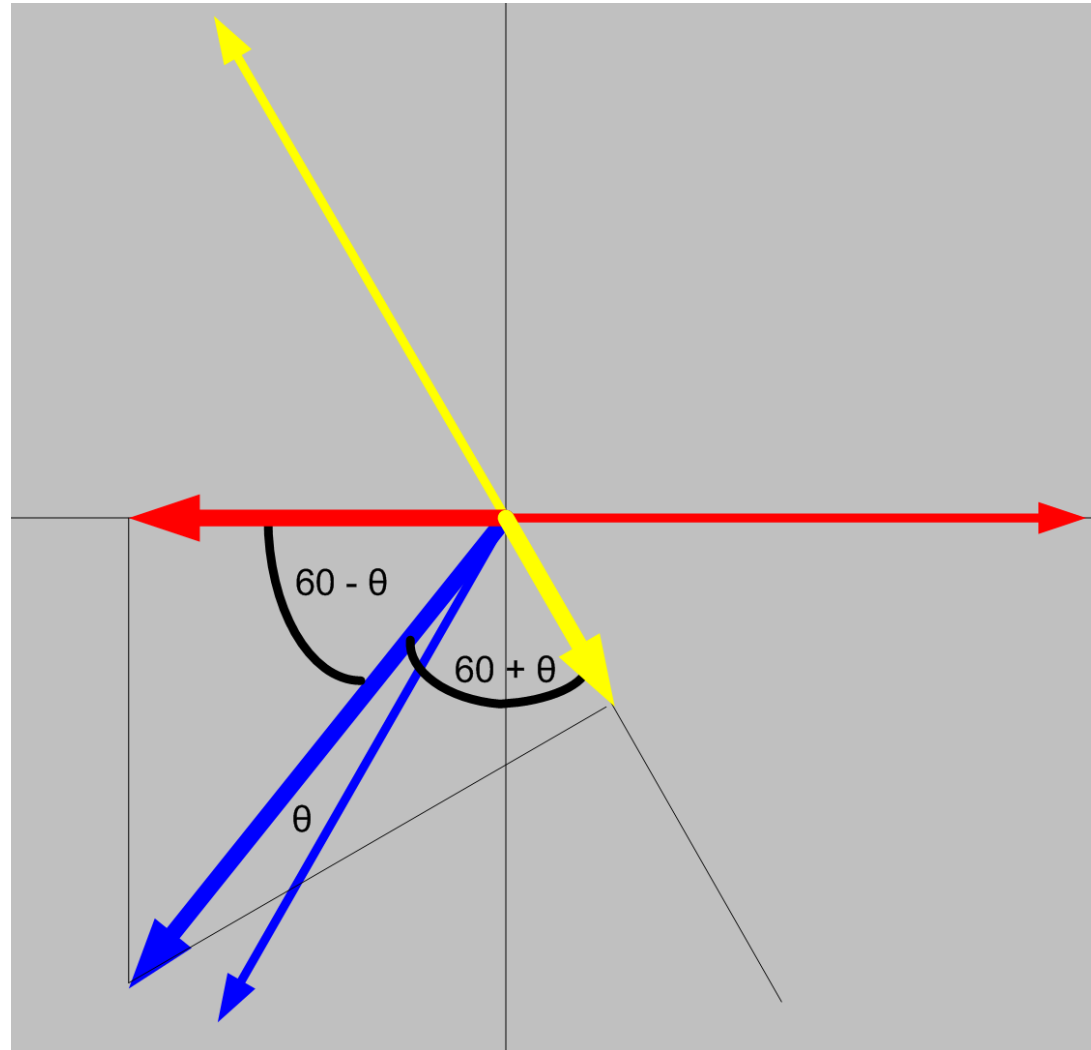
- Four wires
- Two voltage measurements to neutral
- Current measurements on lines 1 & 3.  
How about line 2?

**This DOES NOT satisfy Blondel's  
Theorem.**

# Blondel's Theorem

- In the previous example:
  - What are the “ASSUMPTIONS”?
  - When do we get errors?

# Blondel's Theorem



# Blondel's Theorem

- Phase B power would be:
  - $P = V_b I_b \cos \theta$
- But we aren't measuring  $V_b$
- What we are measuring is:
  - $I_b V_a \cos(60 - \theta) + I_b V_c \cos(60 + \theta)$
- $\cos(\alpha + \beta) = \cos(\alpha)\cos(\beta) - \sin(\alpha)\sin(\beta)$
- $\cos(\alpha - \beta) = \cos(\alpha)\cos(\beta) + \sin(\alpha)\sin(\beta)$
- So

# Blondel's Theorem

- $P_b = I_b V_a \cos(60 - \theta) + I_b V_c \cos(60 + \theta)$
- Applying the trig identity
  - $I_b V_a (\cos(60) \cos(\theta) + \sin(60) \sin(\theta))$   
 $I_b V_c (\cos(60) \cos(\theta) - \sin(60) \sin(\theta))$
  - $I_b (V_a + V_c) 0.5 \cos(\theta) + I_b (V_c - V_a) 0.866 \sin(\theta)$
- Assuming
  - Assume  $V_b = V_a = V_c$
  - And, they are exactly  $120^\circ$  apart
- $P_b = I_b (2V_b) (0.5 \cos \theta) = I_b V_b \cos \theta$

# Blondel's Theorem

- If  $V_a \neq V_b \neq V_c$  then the error is
- %Error =  
$$-I_b \left\{ \frac{V_a + V_c}{2V_b} - \frac{(V_a - V_c) 0.866 \sin(\theta)}{V_b \cos(\theta)} \right\}$$

How big is this in reality? If

$V_a=117, V_b=120, V_c=119, PF=1$  then  $E=-1.67\%$

$V_a=117, V_b=116, V_c=119, PF=.866$  then  $E=-1.67\%$



# AC Theory – Power

- Power is defined as  $P = VI$
- Since the voltage and current at every point in time for an AC signal is different, we have to distinguish between instantaneous power and average power. Generally when we say “power” we mean average power.
- Average power is only defined over an integer number of cycles.

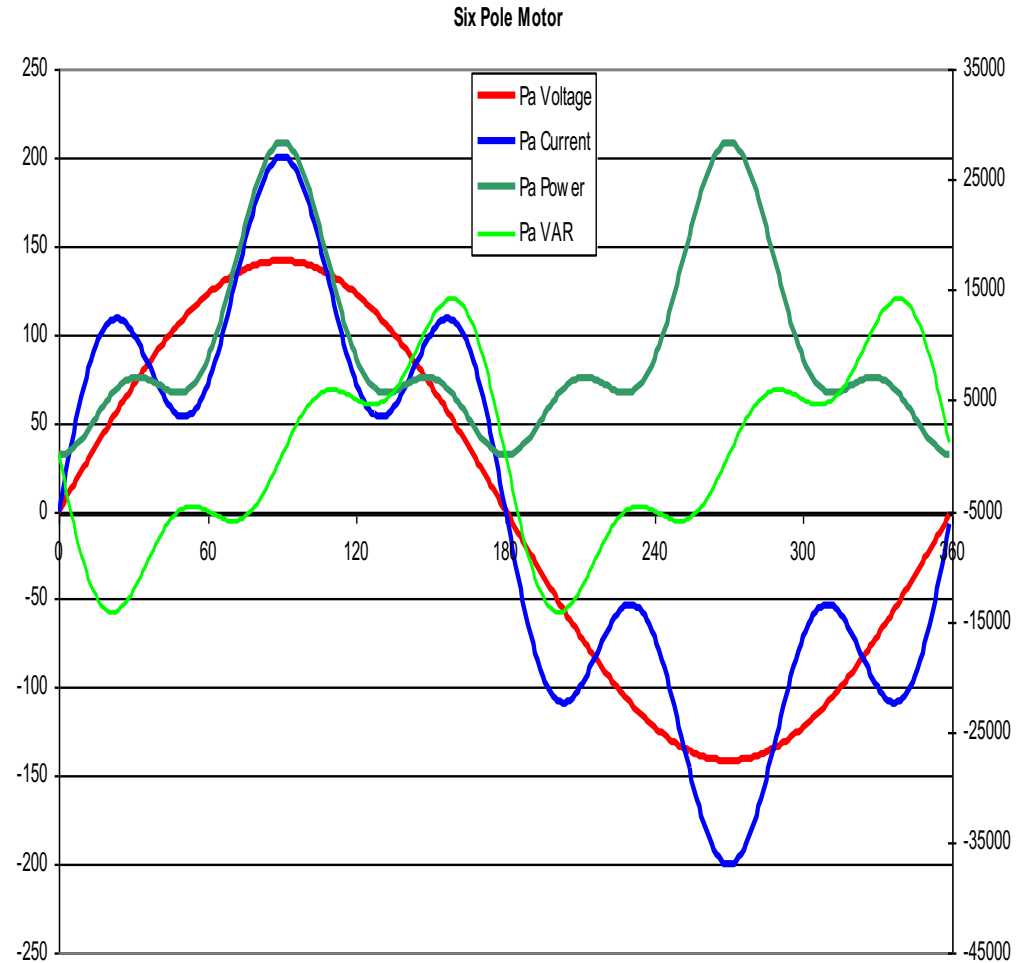
# Harmonics

## Curse of the Modern World

- Every thing discussed so far was based on “Linear” loads.
  - For linear loads the current is always a simple sine wave.  
Everything we have discussed is true.
- For nearly a century after AC power was in use ALL loads were linear.
- Today, many loads are NON-LINEAR.

# Harmonic Load Waveform

Eq.#	Quantity	Phase A
1	V(rms) (Direct Sum)	100
2	I(rms) (Direct Sum)	108
3	V(rms) (Fourier)	100
4	I(rms) (Fourier)	108
5	$P_a = (\int V(t)I(t)dt)$	10000
6	$P_b = \frac{1}{2}\sum V_n I_n \cos(\theta)$	10000
7	$Q = \frac{1}{2}\sum V_n I_n \sin(\theta)$	0.000
8	$S_a = \text{Sqrt}(P^2 + Q^2)$	10000
9	$S_b = V_{rms} * I_{rms}(DS)$	10833
10	$S_c = V_{rms} * I_{rms}(F)$	10833
13	$PF = P_a/S_a$	1.000
14	$PF = P_b/S_b$	0.923
15	$PF = P_b/S_c$	0.923



$$V = 100\sin(\omega t) \quad I = 100\sin(\omega t) + 42\sin(5 \omega t)$$

# Harmonic Load Waveform

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7	$Q = \frac{1}{2}\sum V_n I_n \sin(\theta)$	0.000
8	$S_a = \text{Sqrt}(P^2 + Q^2)$	10000
9	$S_b = V_{rms} * I_{rms}(DS)$	10833
10	$S_c = V_{rms} * I_{rms}(F)$	10833
13	$PF = P_a/S_a$	1.000
14	$PF = P_b/S_b$	0.923
15	$PF = P_b/S_c$	0.923

- Important things to note:

- Because the voltage is NOT distorted, the harmonic in the current does not contribute to active power.
- It does contribute to the Apparent power.
- Does the Power Triangle hold

$$S? = \sqrt{P^2 + Q^2}$$

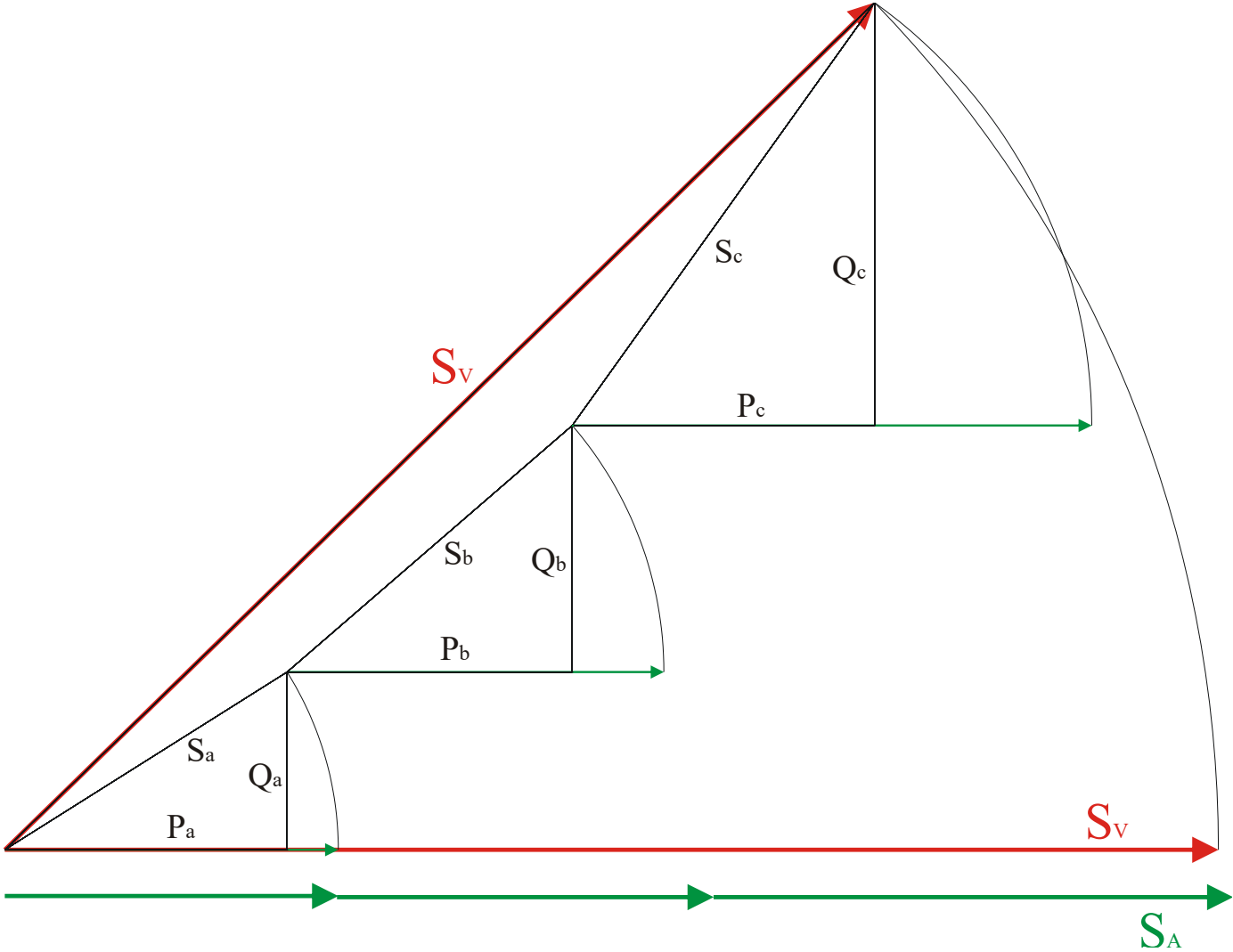
- There is considerable disagreement about the definition of various power quantities when harmonics are present.

$$V = 100\sin(\omega t) \quad I = 100\sin(\omega t) + 42\sin(5 \omega t)$$

# 3 Phase Power Measurement

- We have discussed how to measure and view power quantities (W, VARs, VA) in a single phase case.
- How do we combine them in a multi-phase system?
- Two common approaches:
  - Arithmetic
  - Vectorial

# 3 Phase Power Measurement

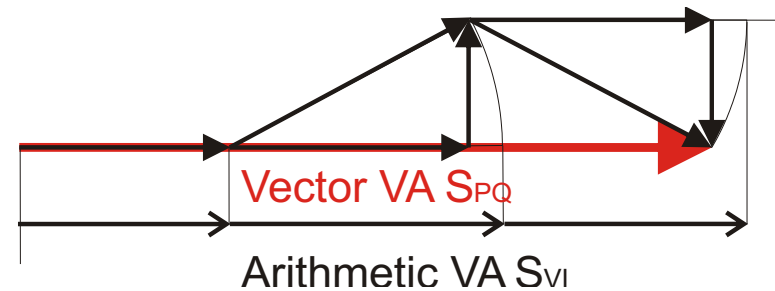


# 3 Phase Power Measurement

- VAR and VA calculations can lead to some strange results:
  - If we define

$$VA = \sqrt{(W_A + W_B + W_C)^2 + (Q_A + Q_B + Q_C)^2}$$

PH	W	Q	VA
A	100	0	100
B	120	55	132
C	120	-55	132
Arithmetic VA			364
Vector VA			340

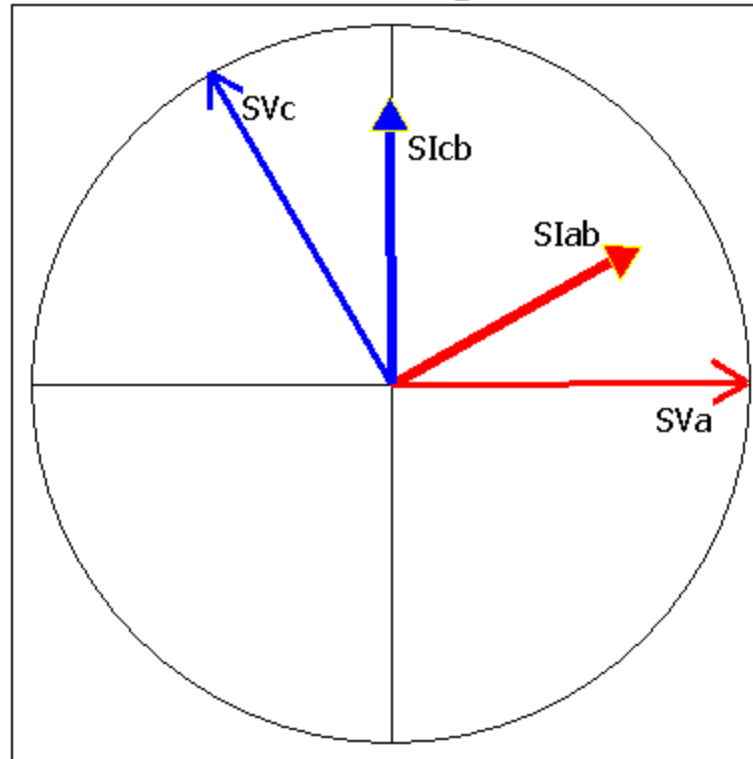


# 3 Phase Power Measurement

Vector Graph

BETA TEST - p19.00M/v17.25M/c#267.23K - Selected Site: ZCOIL

### Vector Diagram



#### $\Phi$ SVaSIab

SVa	118.410	0.00°
SIab	4.354	331.40°
PF =	0.878	-28.60°
Lead		

#### $\Phi$ SVcSIcb

SVc	119.582	239.65°
SIcb	4.386	269.82°
PF =	0.865	30.16°
Lag		

#### SYS

Vsys =	118.996
Isys =	4.370
PF =	0.871
ROT =	ABC

Measurement: Live Test, Sec V/Sec I, Instantaneous

Reference | Connect.View | Interval | Sec V/Pri I | Stop

Arithmetic Calculation - Form 6 – 4 Wire Y Site  
Voltages and Currents Aligned at 0°

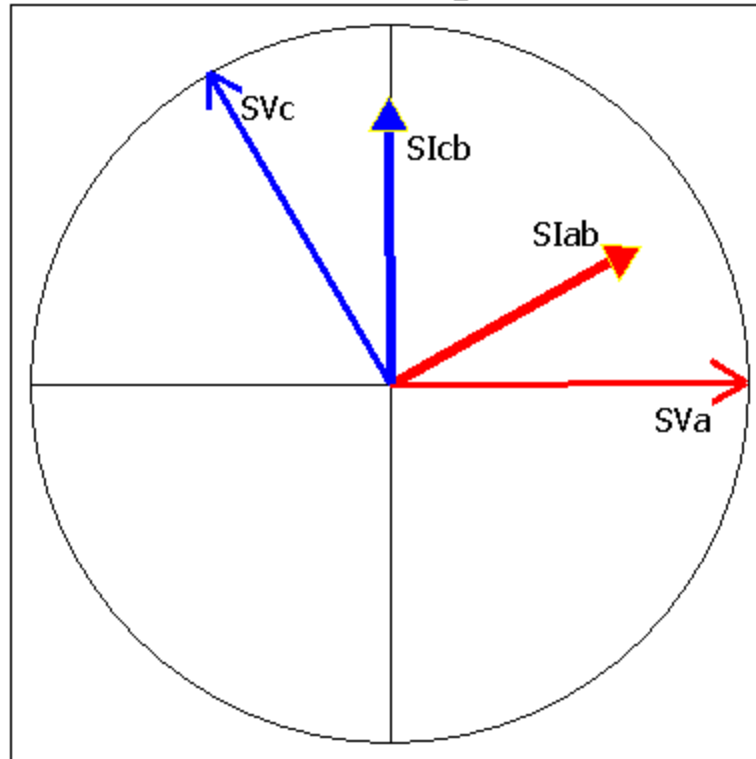


# 3 Phase Power Measurement

Vector Graph

BETA TEST - p16.02M/y16.13M/c#289.54K - Selected Site: ZCOIL

### Vector Diagram



$\Phi$ SVaSIab		
SVa	118.415	0.00°
SIab	4.326	331.34°
PF =	0.877	-28.66°
Lead		

$\Phi$ SVcSIcb		
SVc	119.616	239.74°
SIcb	4.353	269.76°
PF =	0.866	30.02°
Lag		

SYS	
Vsys =	119.015
Isys =	4.339
PF =	1.000
ROT =	ABC

Measurement: Live Test, Sec V/Sec I, Instantaneous

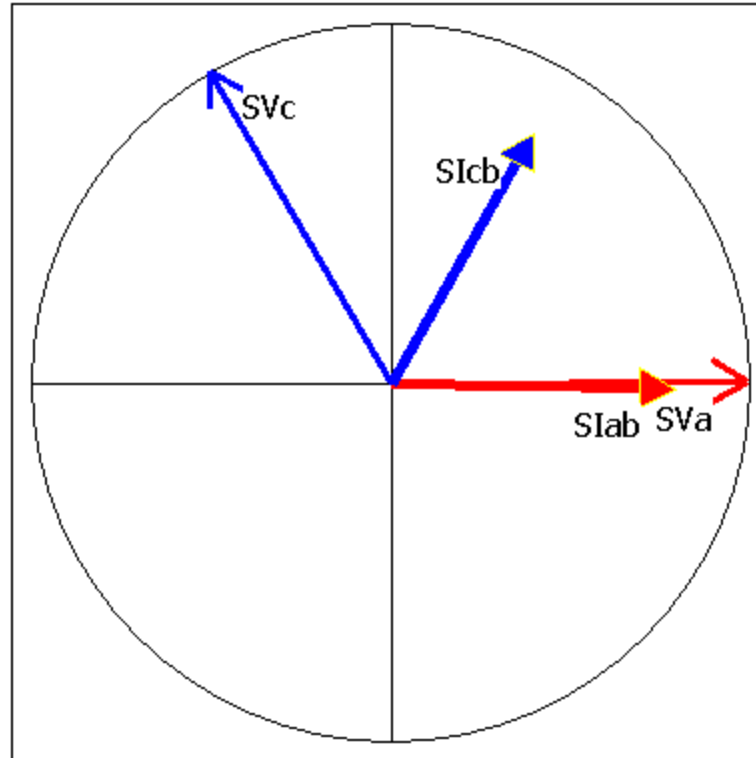
Reference | Connect.View | Interval | Sec V/Pri I | Stop

Vector Calculation - Form 6 – 4 Wire Y Site  
Voltages and Currents Aligned at 0°

# 3 Phase Power Measurement

Vector Graph BETA TEST - p19.00M/v17.25M/c#267.23K - Selected Site: ZCOIL

### Vector Diagram



$\Phi$ SVaSIab		
SVa	118.410	0.00°
SIab	4.346	1.35°
PF =	1.000	1.35°
Lag		

$\Phi$ SVcSIcb		
SVc	119.595	239.68°
SIcb	4.376	299.77°
PF =	0.499	60.09°
Lag		

SYS	
Vsys =	119.002
Isys =	4.361
PF =	0.749
ROT =	ABC

Measurement: Live Test, Sec V/Sec I, Instantaneous

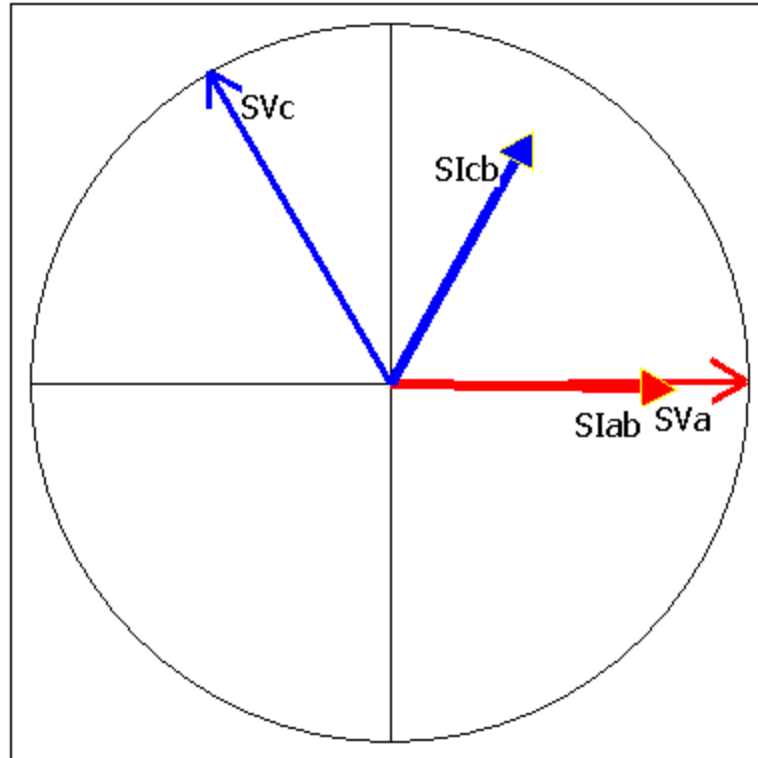
Reference | Connect.View | Interval | Sec V/Pri I | Stop

Arithmetic Calculation - Form 6 – 4 Wire Y Site  
Currents All shifted by 30°

# 3 Phase Power Measurement

Vector Graph BETA TEST - p16.02M/v16.13M/c#289.54K - Selected Site: ZCOIL

## Vector Diagram



$\Phi$ SVaSIab		
SVa	118.420	0.00°
SIab	4.328	1.34°
PF =	1.000	1.34°
Lag		

$\Phi$ SVcSIcb		
SVc	119.596	239.68°
SIcb	4.355	299.75°
PF =	0.499	60.08°
Lag		

SYS	
Vsys =	119.008
Isys =	4.341
PF =	0.857
ROT =	ABC

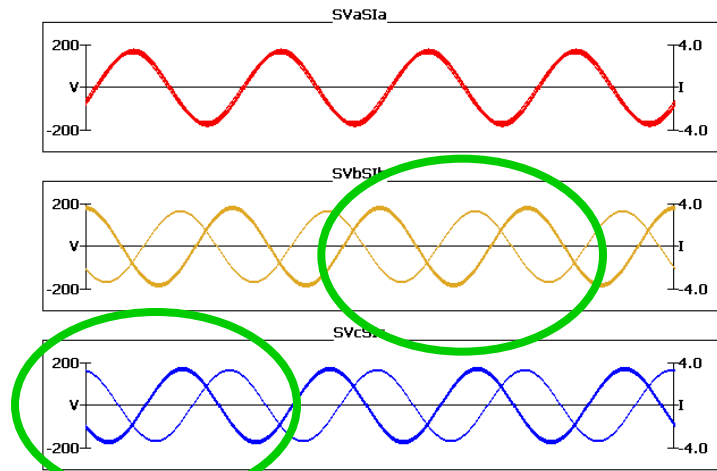
Measurement: Live Test, Sec V/Sec I, Instantaneous

Reference Connect.View Interval Sec V/Pri I Stop

Vector Calculation - Form 6 – 4 Wire Y Site  
 Currents All shifted by 30°

# Actual Field Test Case #1: Lots of Clues!

Waveform Analysis BETA TEST - p22.63M/v20.19M/c#224.81K - Selected Site: \*NONE\*



Measurement: Live Test, Sec V/Sec I, Instantaneous

Single Sec V/Pri I Stop

Power Meter BETA TEST - p22.61M/v20.19M/c#224.81K - Selected Site: \*NONE\*

## SYSTEM OVERALL SUMMARY

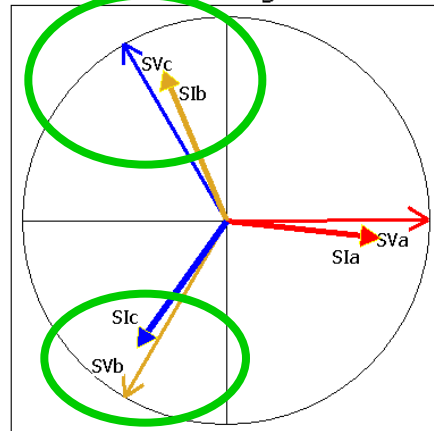
	$\Phi$ SVaSIa	$\Phi$ SVbSIb	$\Phi$ SVcSIc	SYSTEM
V(FDRMS)	118.6084	119.4340	119.7152	119.2526
V(Fund)	118.6021	119.4339	119.7151	119.2504
I(FDRMS)	2.487482	2.602328	2.469598	2.519800
A(Fund)	2.487467	2.602313	2.469585	2.519788
$V\theta$	0.0000°	119.8120°	239.8798°	
$I\theta$	6.3062°	247.3043°	124.8261°	
DPF $\theta$	6.3062°	127.4923°	-115.0537°	
PF(PF1a)	0.993949	0.608656	0.423469	0.675358
<b>W(P1)</b>	<b>293.2338</b>	<b>-160.1729</b>	<b>-125.1972</b>	<b>-21.1364</b>
VA(S1)	295.0188	-310.8044	295.6465	-311.4321
VAR(Qt)	32.4005	246.6024	-267.8293	11.1736
THD V	1.033658%	0.138453%	0.142976%	0.438362%
THD I	0.338860%	0.232847%	0.328474%	0.300060%
FREQ	60.00016	60.00016	60.00015	60.00016

Measurement: Live Test, Sec V/Sec I, Instantaneous

Interval Sec V/Pri I Stop

Vector Graph BETA TEST - p24.11M/v20.19M/c#225.06K - Selected Site: \*NONE\*

## Vector Diagram



$\Phi$ SVaSIa		
SVa	118.611	0.00°
SIa	2.488	6.30°
PF =	0.994	6.30°
Lag		

$\Phi$ SVbSIb		
SVb	119.436	119.80°
SIb	2.602	247.29°
PF =	0.609	127.49°
Lag		

$\Phi$ SVcSIc		
SVc	119.715	239.87°
SIc	2.469	124.83°
PF =	0.423	-115.04°
Lead		

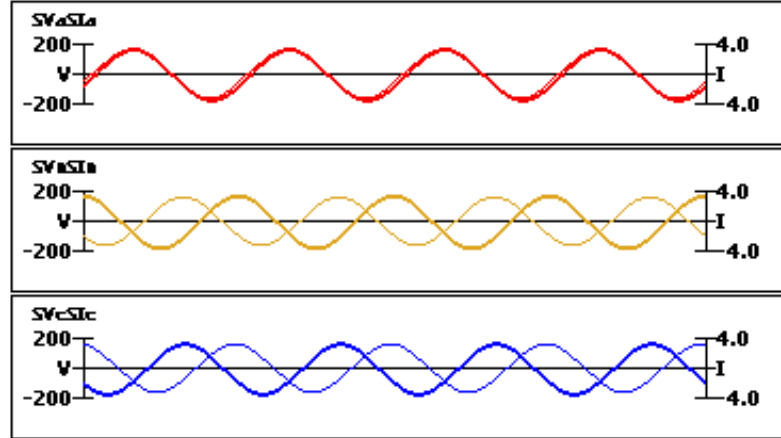
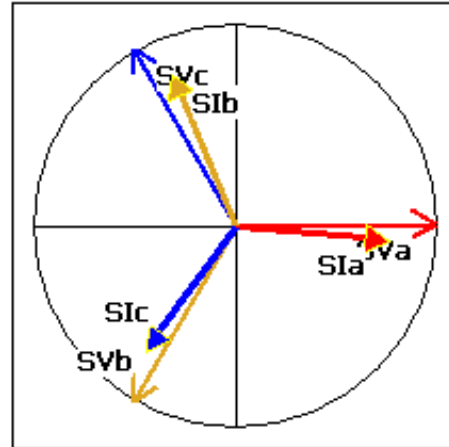
SYS	
Vsys =	119.254
Isys =	2.520
PF =	0.675
ROT =	ABC

Measurement: Live Test, Sec V/Sec I, Instantaneous

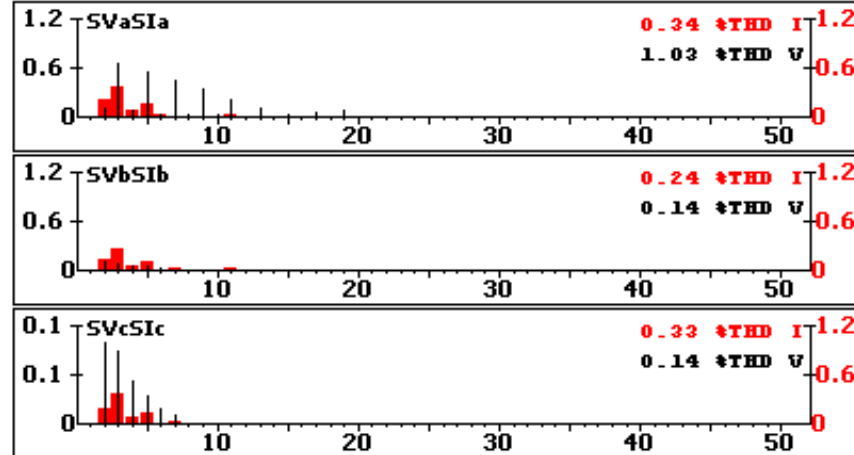
Reference Show Wiring Interval Sec V/Pri I Stop

# Actual Field Test Case #1: Lots of Clues!

Full Analysis BETA TEST - p22.60M/v20.19M/c#224.81K - Selected Site: \*NONE\*



	$\phi_{SVaSIa}$	$\phi_{SVbSIb}$	$\phi_{SVcSIc}$	SYSTEM
V(FDRMS)	118.62	119.43	119.71	119.25
V(Fund)	118.61	119.43	119.71	119.25
I(FDRMS)	2.4872	2.6023	2.4696	2.5197
A(Fund)	2.4872	2.6023	2.4696	2.5197
$V\theta$	0.00°	119.81°	239.88°	
$I\theta$	6.30°	247.30°	124.83°	
DPF $\theta$	6.30°	127.49°	-115.06°	
PF(PF1a)	0.9940	0.6086	0.4235	0.6754
<b>W(P1)</b>	<b>293.22</b>	<b>-189.16</b>	<b>-125.21</b>	<b>-21.15</b>
VA(S1)	295.00	-310.80	-295.65	-311.44
VAR(Qt)	32.39	246.60	-267.82	11.17
THD V	1.0255%	0.1385%	0.1430%	0.4356%
THD I	0.3445%	0.2373%	0.3332%	0.3050%
FREQ	60.000	60.000	60.000	60.000



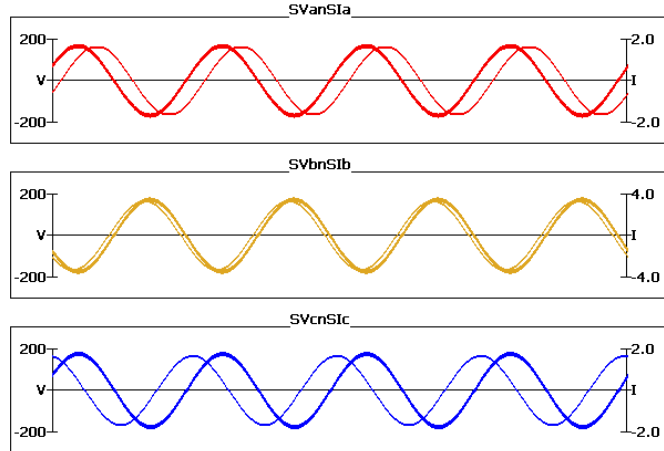
Measurement: Last Test, Sec V/Sec I, Instantaneous

Restart

**Phase B & C reversed!**

# Actual Field Test Case #2:

Waveform Analysis BETA TEST - p21.10M/v19.06M/c#275.45K - Selected Site: DELETE



Measurement: Last Test, Sec V/Sec I, Instantaneous

Save

Power Meter BETA TEST - p21.10M/v19.06M/c#275.40K - Selected Site: DELETE

## SYSTEM OVERALL SUMMARY

	ΦSVanS1a	ΦSVbnS1b	ΦSVcnS1c	SYSTEM
V(FDRMS)	118.5131	119.4399	119.7201	119.2244
V(Fund)	116.3053	119.4398	119.7206	119.2217
I(FDRMS)	1.205595	2.489768	1.263508	1.652957
A(Fund)	1.205588	2.489754	1.263505	1.652949
VØ	0.0000°	119.8231°	239.8896°	
IØ	312.8747°	132.6724°	314.2653°	
DPFØ	-47.12535°	12.84930°	74.37667°	
PF(PF1a)	0.680394	0.974958	0.269311	0.641554
<b>W(P1)</b>	<b>97.2070</b>	<b>289.9290</b>	<b>40.7378</b>	<b>427.8738</b>
VA(S1)	142.8686	297.3758	151.2668	591.5112
VAR(Qt)	-104.6986	66.1333	145.6779	107.1126
THD V	1.148540%	0.140896%	0.145333%	0.478256%
THD I	0.347228%	0.332820%	0.221998%	0.300682%
FREQ	59.99932	60.00014	60.00013	59.99986

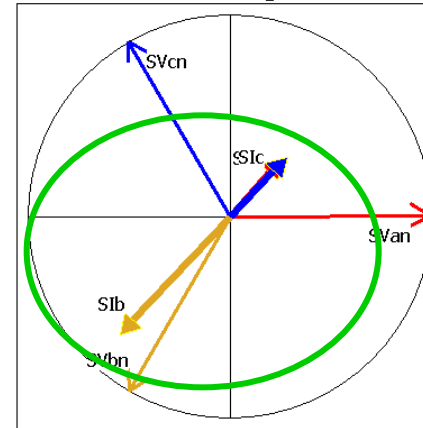
Measurement: Last Test, Sec V/Sec I, Instantaneous

Save

$$I_b = I_a + I_c$$

Vector Graph BETA TEST - p21.10M/v19.06M/c#275.40K - Selected Site: DELETE

## Vector Diagram



ΦSVanS1a

SVan	118.505	0.00°
SIa	1.206	312.87°
PF =	0.680	-47.13°
Lead		

ΦSVbnS1b

SVbn	119.440	119.82°
SIb	2.490	132.67°
PF =	0.975	12.85°
Lag		

ΦSVcnS1c

SVcn	119.720	239.89°
SIc	1.264	314.27°
PF =	0.269	74.38°
Lag		

SYS

Vsys =	119.222
Isys =	1.653
PF =	0.642
ROT =	ABC

Measurement: Last Test, Sec V/Sec I, Instantaneous

Save

I<sub>b</sub> opposite to I<sub>a</sub> & I<sub>c</sub>

Customer Load Test Results A TEST - p21.14M/v19.00M/c#275.08K - Selected Site: DELETE

## Customer Load Meter Test Wh Test

**% Registration 100.015**

### Test Info

Time(sec)	151.427
Time Left	0.000
Pulses Exp	9.9985
Pulses Act	10.0000
Meter PF	0.6416

### Sys Info

Wh	17.9973
VAh	24.8777
VARh	4.4997
V	119.259
I	1.6524

Test Complete

Restart

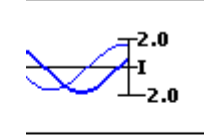
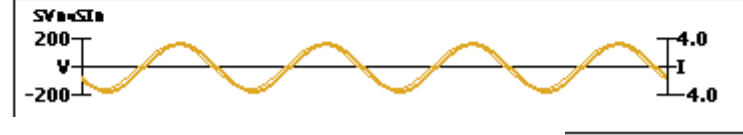
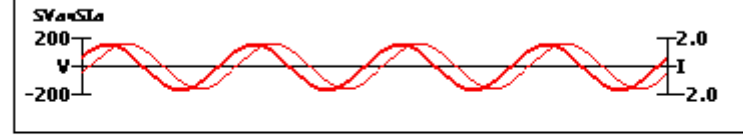
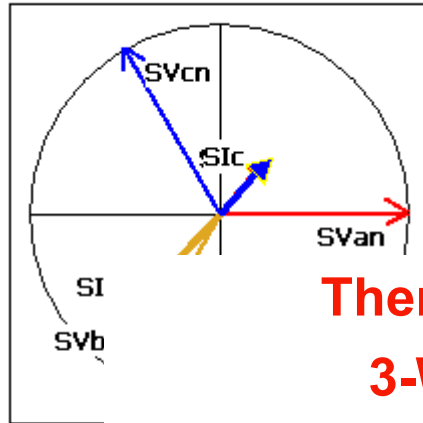
View Trend

Registration OK!



# Actual Field Test Case #4:

Full Analysis BETA TEST - p21.10M/v19.06M/c#275.40K - Selected Site: DELETE

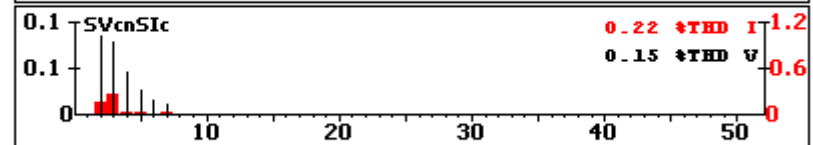
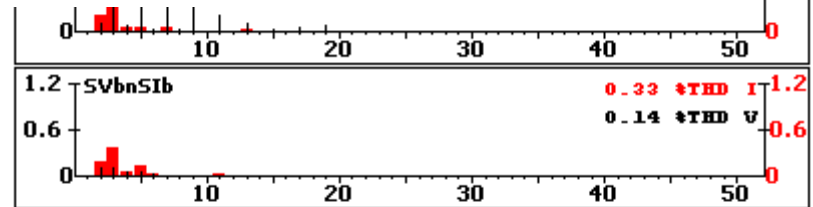
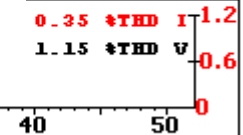


There is no problem!

3-Wire Delta load

On a 4-Wire Wye service.

V(FDRMS)				
V(Fund)	119.72	119.77	119.76	119.66
I(FDRMS)	1.2056	2.4898	1.2635	1.6530
A(Fund)	1.2056	2.4898	1.2635	1.6529
V@	0.00°	119.82°	239.89°	
I@	312.87°	132.67°	314.27°	
DPF@	-47.125°	12.849°	74.377°	
PF(PF1a)	0.6804	0.9750	0.2693	0.6416
<b>W(P1)</b>	<b>97.21</b>	<b>289.93</b>	<b>40.74</b>	<b>427.87</b>
VA(S1)	142.87	297.38	151.27	591.51
VAR(Qt)	-104.70	66.13	145.68	107.11
THD V	1.1485%	0.1409%	0.1453%	0.4783%
THD I	0.3472%	0.3328%	0.2220%	0.3007%
FREQ	59.999	60.000	60.000	60.000



Measurement: Last Test, Sec V/Sec I, Instantaneous

What is the problem?

**Questions? Comments?**

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**Thank you for your time!**

